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HIGH LATITUDE MODELS, OBSERVATIONS, AND ANALYSIS OF IONOSPHERIC SCINTILLATIONS

Jules Aarons, et al

Air Force Cambridge Research Laboratories L. G. Hanscom Field, Massachusetts

12 January 1973

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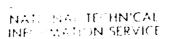
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JULES AARONS HERBERT E. WHITNEY RICHARD S. ALLEN DOUGLAS R. SEEMANN

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#### AIR FORCE CAMBRIDGE RESEARCH LABORATORIES

L. G. HANSCOM FIELD, BEDFORD, MASSACHUSETTS

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#### **Abstract**

In order to provide systems engineers with observations and analysis of the amplitude-fading of radio waves traversing the high intude ionosphere, several different studies were performed. The concept was to the descriptive and statistical models for the pattern of occurrence and amplitude of ccintillations at high latitudes. Then, long term observations from a limited number of sites could be linked to allow an assessment of the scintillation problem to communication, navigation, and detection systems in the VHF and UHF bands. This report discusses these studies in three chapters. In Chapter 1, general patterns of scintillation occurrence and intensity are presented in the descriptive model of the F-layer irregularities at high latitudes. This is followed in Chapter 2 by a graphical presentation of the data; that is, observations of the 136 MHz beacon of ATS-3. Chapter 3 organizes the observations into a useful format-the cumulative amplitude probability distribution function-for the engineer. A means of adjusting the observations for frequency dependence is provided. Cumulative amplitude probabilities are listed for Sagamore Hill, Massachusetts and Narssarssuaq, Greenland as a function of season, time and K index. For Thule, Greenland cumulative amplitude probability distributions are listed for ATS-3 at 136 MHz. With this data and with the descriptive model, it is proposed that the engineer can evaluate the effect of scintillations on systems operating in auroral and polar regions.

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## HIGH LATITUDE MODELS, OBSERVATIONS, AND ANALYSIS OF IONOSPHERIC SCINTILLATIONS

## 1. A Descriptive Model of F-Layer High Latitude Irregularities

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#### **Abstract**

Using observations of the amplitude fluctuations of radio signals from satellites and radio stars as a data base, a model is sketched of the high latitude F-layer irregularity region. The irregularities of concern are field aligned and small scale (1 to 10 km). On the nightside, irregularity intensity increases from a low level—at its equatorward boundary position of ~57° at 2200 local time—to a higher level within the auroral oval. A high level of irregularity intensity excess over the corrected geomagnetic pole. The data base for quantitative measis, ments at latitudes poleward of the auroral oval, however, is small. On the layside, the scintillation boundary is in the region of 70° for quiet to moderate magnetic conditions.

During all hours an increase in magnetic activity brings on deeper fading across the entire high latitude region, from the equatorward scintillation boundary to the geomagnetic pole.

Precipitation of electrons, with energies of the order of a few hundred eV, is not thought to be the mechanism for the production of small scale irregularities. In this energy range, electron precipitation shows a low occurrence in the polar cavity while scintillations remain high in this region.

Measurements of suprathermal electrons show polar patterns closer to the scintillation observations than measurements of high energy electrons. Irregularities observed in thermal-electron satellite observations (R. Sagalyn, private

(Received for publication 10 January 1973)

communication, 1973) at high latitudes—including polar areas—show geomagnetic occurrence patterns—together with those in polar areas—similar to the ones shown in this paper. In their measurements of turbulent isotropic electric fields at 400 km, Kelley and Mozer (1972) have found variations with latitude in the boundary region, the amoral oval and over the pole which resemble those postulated in this model.

#### 1.1 INTRODUCTION

At high latitudes, small scale (1 to 10 km) field-aligned irregularities in the F layer have been detected by many techniques. These include bottom and topside sounders, scintillation recordings of radio stars and satellite beacons, and in r.tu Langmuir probes and vector electric field detectors.

The model of high-latitude irregularity morphology to be presented stems from a critical evaluation of published and new material on scintillations. The sketch of the model takes its form from the detection technique employed. In this case, the perspective is dictated by data available from diffraction observations of radio signals as they traverse the ionospheric holes or enhancements.

Other views of the irregularity scene have emerged using different perspectives. Spread F measurements, made by ground ionosounders, are severely limited at high latitudes by strong absorption during proton events and during periods of auroral absorption. In addition, spread F returns are screened by E-layer auroral reflections and by sporadic E. Topside soundings display only those F-layer irregularities above the peak of the F layer. In commonly available observations of both topside and bottomside soundings, only occurrence or non-occurrence of spread F is available; quantitative values are not given.

Scintillation data is quantitative in its scaling. New analyses (Whitney et al, 1972) have allowed frequency dependence scaling to be performed. The combination of radio star observations, low-altitude (1000 km) satellite transmissions, and synchronous satellite observations had produced a mix of elevation angles, snapshots of the irregularity structure, and long-term synoptic measurements which can be assembled into a model.

In addition to irregularities produced at high latitudes by processes related to magnetospheric causation, other types of irregularities at both E and F layers produce scintillations. These include isolated F-layer patches (Slack, 1972) and sporadic E of the spread type (Anastassiadis et al. 1970 and Chen et al. 1972). These can be of importance at latitudes in the region of  $55^{\circ}$  or lower, but their occurrence pattern and the magnitude of their offect on signals in the 100 MHz range and higher is less than the effect of magnetospherically-associated, high-latitude irregularities in the auroral and polar cap regions.

In this paper, one will notice that a large percentage of the observations being used consists of data from the observatories associated with the author. The rationale is that the data have been analyzed in consistent quantitative terms, are available for satisfical manipulation, and fall along a relatively narrow longitudinal swath (51° to 71° West, except for a small amount of data from Alaska).

The records were reduced by the method given by Whitney et al (1969) into 15-min scintillation indices. In this system, a scintillation index of 40 represents a +1.5 dB to -2.2 dB excursion from mean quiet level; an index of 60 represents +2 dB to -4 dB.

Figure 1.1 is an outline of the general form of the irregularity region during periods of very quiet magnetic activity, Kp = 0, 1, and for one disturbed magnetic

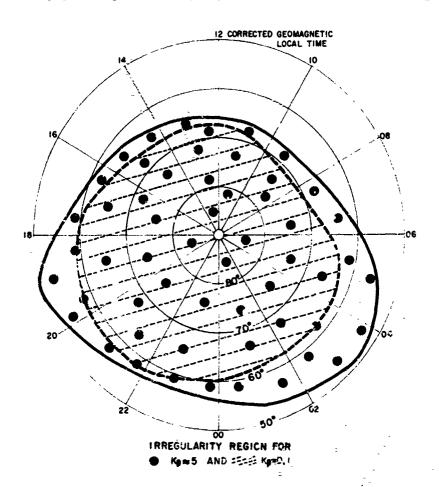


Figure 1. 1. Diurnal Pattern of the Extent of the F-Layer Irregularity Region During Quiet Magnetic Conditions (Kp = 0, 1) and for Kp  $\approx 5$ 

index, ( $Kp \approx 5$ ) (in the text that follows, index K only is used). This paper will describe the variations of the boundary or the irregularity region, the change of intensity of the irregularities within the region, and the occurrence of irregularities within the polar cap. We have assumed that the irregularities are at F-iayer heights; the work of Lizka (1964) and Frihagen (1969), as well as others, has established the region between 250 and 500 km as the predominant height range for the irregularities that produce scintillations.

#### 1.2 THE LOWER BOUNDARY

#### 1.2.1 Night Observations

#### 1.2.1.1 MAGNETICALLY QUIET CONDITIONS

By statistically analyzing observations of Transit 4A scintillations at 54 MHz, it was determined (Aarons et al, 1969) that the scintillation boundary had an oval form, differing substantially in both latitudinal peregrinations and precise positions from the optically derived E-layer auroral oval. The boundary falls to 57° invariant latitude at 2200 local time for K = 0, 1; the auroral oval has a lower boundary of 60° for the same magnetic conditions (Feldstein and Starkov, 1967). The definition of the lower latitude of the irregularity region, termed the scintillation boundary, was arbitrary in one sense; that is, it was chosen as the latitude at which the mean scintillation index at 40 MHz reached or exceeded 50 percent. It corresponded, however, to the latitude where the sudden onset of irregularities was coserved. In that sense, it is the boundary between the ordered F layer and the irregularity region.

Recent papers have brosply verified the midnight boundary position. Oksman and Tauriainen (1971) found a boundary latitude of  $59^{\circ}$  for  $K \leq 3$  shortly after midnight. Kersley et al (private communication, 1971) found a scintillation boundary of  $54^{\circ}$  shortly before midnight for K = 0, 1. Kaiser and Preddey (1968) found somewhat lower transition latitudes around midnight in the southern hemisphere.

It should be stressed that the irregularity region's equatorward boundary is statistical. It may move to latitudes higher than those shown in Figure 1.1 for K = 0, 1. When the K index remains consistently low over a period of days, Aarons et al (1972) have shown that the midnight boundary may retreat to latitudes higher than  $64^{\circ}$ .

In Figure 1.2, the mean scintillation index at 136 MHz is plotted as a function of invariant latitude for the broad local time period 2200-0200, and for quiet (0, 1), moderate (2, 3), and disturbed (4-9) conditions. The genesis of this diagram will be outlined as individual time periods and magnetic conditions are examined.

For K=0, 1 the irregularity region starts abruptly at  $60^{\circ}$  with an index of  $\sim 8$  percent (which corresponds to an index of 50 at 40 MHz). The intensity of the irregularities

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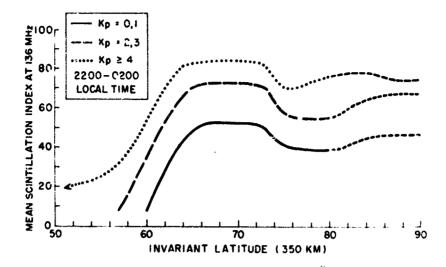


Figure 1.2. Idealized Curves of the Variations With Latitude of Mean Scintillation Index at 136 MH: as a Function of Kp. The values are given for the local time period of 2200-0200

increases with latitude up to 66°, remaining constant until 73°, decreasing slightly in a trough region but increasing over the pole to a value slightly below its auroral oval level. We have used broad dashes above 80° to indicate the uncertainty in values due to the sparcity of data for this region.

A great deal of data is available for the latitudinal region 50° to 64°, somewhat less for the region 54° to 82°, and very little for the region 82° to the pole. Night measurements in the lower portion of the irregularity region are plentiful, due to the high occurrence of observatories at middle and auroral latitudes.

#### 1. 2. 1. 2 MAGNETICALLY DISTURBED CONDITIONS

When magnetic conditions become disturbed, two effects can be noted (see Figure 1.2):

- (1) Boundary Motion: During periods of magnetic disturbance, the boundary of the irregularity region drops to lower latitudes. Aarons and Allen (1971) have shown that the maximum change—2 to  $2.5^{\circ}/\mathrm{K}$ —in the nighttime equatorward boundary, as a function of K index, took place between 0200 and 0600 local time. The nightly mean was a  $1^{\circ}/\mathrm{K}$  lowering of the boundary latitude.
- (2) Increase in Index: Mean scintillation index increases throughout the entire auroral and polar region during periods of magnetic disturbance, although the percentage of increase may vary as a function of latitude. From the evidence of scintillation measurements, there is no indication of a polar cavity in the occurrence of deep scintillation at any time.

In the region between the boundary and below the quiet auroral oval, the depth of scintillation was determined by comparisons of many measurements; these included zenithal observations of Cassiopeia at 113 MHz (Aarons and Allen, 1966), and a comparison study of satellite beacon and radio star measurements (Basu et al. 1964).

#### 1.2.2 Day Observations

Through a recent analysis of observations of the 40 MHz transmissions of BE-B taken at Narssarssuaq, Greenland in collaboration with the Danish Meteorological Institute, we have been able to revise the daytime boundary; the revision is incorporated in Figure 1.1. Narssarssuaq, at an invariant latitude of  $69^{\circ}$  (at 350 km) allowed the daytime boundary to be defined for K = 0, 1 and K = 2, 3. The boundary and polar indices at 40 MHz are shown in Figure 1.3 for the noon sector. For this time period, the boundary was between  $71^{\circ}$  and  $76^{\circ}$  for K = 0, 1 and  $68^{\circ}$  to  $69^{\circ}$  for K = 2, 3. It was difficult to determine the precise latitude for the lower K indices since the mean SI showed a plateau for the  $71^{\circ}$  to  $76^{\circ}$  range. At K = 2, 3 the indices rose decisively with latitude and a boundary can be given. From Figure 1.1, it can be seen that the highest equatorward latitude of the irregularity region occurs before noon; there is a distinct assymetry around noon.

In the local time period, 0600-1800, there is a motion of the boundary of approximately 0.50/K. The method of analysis for this data was similar to that used in Aarons and Allen (1971). In the non sector, the auroral oval's equatorward

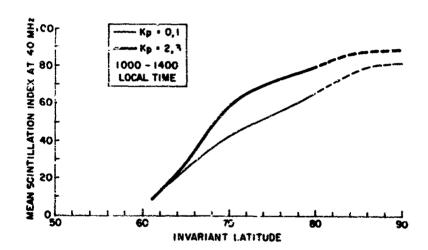


Figure 1.3. Idealized Curves of the Variations With Latitude of Mean Scintillation Index at 40 MHs as a Function of Kp for the 1000-1400 Local Time Period

boundary is  $76^{\circ}$  at Q (polar range index) = 0 and  $69^{\circ}$  for Q = 2; this is a close approximation to scintillation observations.

#### 1.3 THE AURORAL OVAL AND THE POLAR CAP

#### 1.3.1 Vight Observations

In the midnight sector for Q = 0, the aval extends from  $70^{\circ}$  to  $72^{\circ}$  (Feldstein and Starkov, 1967); for Q = 2, the aval extends from  $67^{\circ}$  to  $70^{\circ}$ . Scintillation indices appear to maximize broadly in these regions during periods of magnetic quiet.

Much of the data used to construct the curves in Figure 1.2 comes from ground measurements of the scintillations of various synchronous satellite transmissions at 136 MHz. A schematic drawing of the ground station angles of elevation and intersection latitudes is shown in Figure 1.4. Subionospheric latitudes of 54°, 58°, 60°, and 64° were probed and their data used in this paper. Thule observations at a very low angle of elevation (4°) could not be used quantitatively.

Figure 1.5 compares mean scintillation indices for Sagamore Hill and Narssarssuaq for the same days for  $K=2,3,\ 137$  to 223 points for each hour were used.

Another series of data was available for comparison, but only for the period November 1971 to March 1972 (inclusive). This series for Gocse Bay, Canada, College, Alaska, and Narssarssuaq, Greenland showed that from  $58^{\circ}$  to  $63^{\circ}$ , the change in mean scintillation index—during periods of magnetic quiet—was approximately a factor of 2 for a 2.5° interval. The data for the three stations is shown in Figure 1.6(a) for K = 2,3 and Figure 1.6(b) for K = 0,1.

At 66°, a comparison between quiet and moderately disturbed conditions was made using lower transit measurements of the scintillations of Cassiopeia A made at Sagamore Hill with a 150° parabola. The geometry of these measurements, as well as the geometry of upper transit measurements, is shown in Figure 1.7. For one year, June 1963 to June 1964, observations of scintillations of Cassiopeia A were made at 113 MHz and 228 MHz. This data allowed us to compare two sets of magnetic indices for one intersection latitude, 66°. The 113 MHz data are shown in Figure 1.8. Clearly, at 66° there is an increase in scintillation index when magnetic index increases. Upper transit data taken at Sagamore Hill and reported in Aarons and Allen (1966) were also used in the construction of Figure 1.2. In both uses of radio star data, the ratios of scintillation indices were used rather than absolute values.

An extensive series of measurements is available at  $64^{\circ}$  from Narasarasuaq. This data divided into magnetic index sets of K = 0, 1, K = 2, 3, and K = 4-9

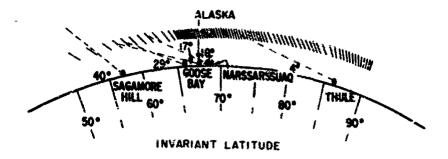


Figure 1.4. Positions of Sites, Intersection Latitudes and Angles of Elevation (for Invariant Latitudes Taken at 350 km) for Observatories Supplying Synchronous Satellite Data Used in This Paper

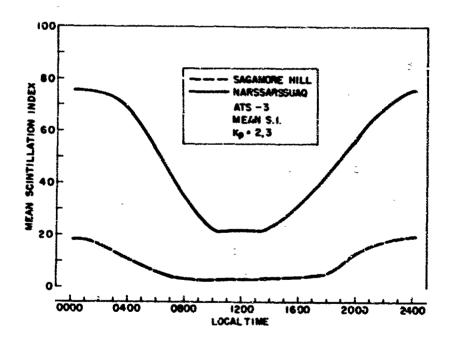


Figure 1.5. Comparison of Mean Scintillation Indices for the Same Hours for Sagamore Hill and Narssarssuaq With Kp = 2,3

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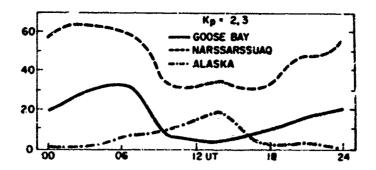


Figure 1.6a. K Indices of 2,3 Yield Higher Values of Scintillation Indices for Both Alaska and Narssarssuaq but Little Change for Goose Bay Observations

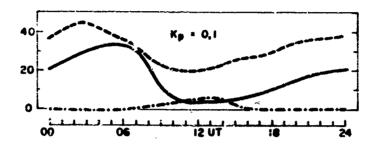


Figure 1.6b. Mean Scintillation Indices for the Same Time Period (November 1971 to March 1972) for Three Stations Situated at High Latitudes. Observations at low K indices (0, 1) are given in this figure

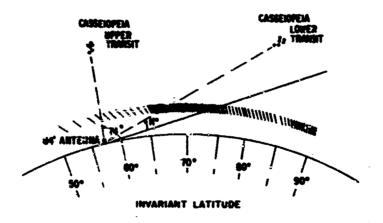


Figure 1.7. The Geometry of Radio Star Scintillation Measurements From Sagamore Hill is Shown. Data from both an 84 It antenna and a 156 It antenna were used in this paper

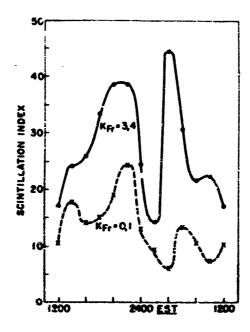


Figure 1.8. Scintillation Indices for 113 MHz Radio Emission From Cassiopeia A. A 150 ft antenna at Sagamore Hill was used to make observations near lower transit (~ 130 of elevation) on a path intersecting the invariant latitude of 660 (at 350 km)

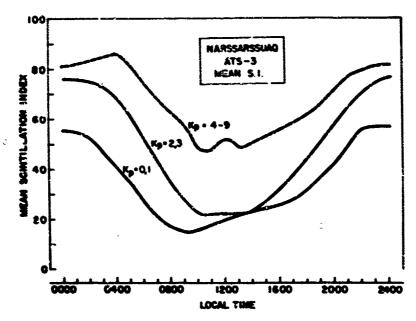


Figure 1.9. Mean Scintillation Indices Recorded at Narssarssuaq, Greenland as a Function of Local Time and K Index. Note both increasing index with increasing K index as well as a shift in time of maximum (towards later local times) with increasing K index

(see Figure 1.9). The difference between the mean values of radio star a id satellite indices is believed to be due to the fact that the radio star data was taken near the minimum in the sunspot cycle, where the satellite data are near maximum. Figure 1.2, therefore, represents sunspot maximum variations with latifude.

#### 1.3.2 Noon Observations

#### 1.3.2.i MAGNETICALLY QUIET CONDITIONS (K = 0,1; K = 2,3)

To construct Figure 1.3, we freely transferred scintillation indices of various types from three sets of high latitude observations. Since the noon boundary begins near 70°, only sites somewhat below this latitude and inside the day portion of the oval and polar cap were useful. Data from the three sites were combined. The sites were Narssarssuaq at 69°, Spitzbergen at 76°, and Thule at 86°. The satellite signal for the three observational sets was the BE-B transmitting at 40 MHz. The scale, therefore, for Figure 1.3 is mean SI at 40 MHz. Since simultaneous high latitude measurements at 40 MHz and 136 MHz signals are available, it is difficult to develop a correction factor.

Equatorward slopes of the curves in Figure 1.3 were obtained from an analysis of the Narssarssuaq data as well as those published by Frihagen (1971), with the latter being taken at Spitzbergen.

At Narssarssuaq, a limited series of measurements of the 136 MHz beacon of the ITOS satellite (orbiting at  $\sim 1000$  km altitude), were reduced. A steep rise was noted during the noon hours at subienospheric paths north of Narssarssuaq ( $71^{\circ}$  to  $72^{\circ}$ ), corroborating qualitatively the more extensive BE-B measurements.

In a series of measurements at 40 MHz from the polar station, Thule, Nielsen and Aarons (unpublished data, 1973) show a rise at all times of the occurrence of deep fading as the Corrected Geomagnetic Pole is approached.

#### 1.3.2.? MAGNETICALLY DISTURBED CONDITIONS

During the magnetic storms, both Frihagen (1971) and Nielsen and Aarons (1973) found increased scintillation indices. In the noon sector for  $K \ge 3$ , Frihagen characterized the scintillations with an index of 4, his highest contour for the latitudinal range  $68^{\circ}$  to  $82^{\circ}$ . At noon, comparing disturbed (K = 4-9) and quiet conditions, Nielsen and Aarons found an increase in occurrence of deep fading by a factor greater than 2 from  $82^{\circ}$  to  $83^{\circ}$ , but a smaller increase from  $88^{\circ}$  to  $90^{\circ}$ .

#### 1.4 ASPECT SENSITIVITY

Two of the principal factors affecting the scintillation index for a particular observatory are aspect sensitivity and angle of elevation. The maximum effect of

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a field-aligned irregularity takes place when the line of sight to the radio source and the alignment of the irregularity in the earth's magnetic field are the same (Singleton, 1970). The effect of aspect sensitivity is a function of the propagation angle and the irregularity characteristics (height, dimensions). Angle of elevation corrections are outlined by Briggs and Parkin (1963); a correction for angle of elevation for large azimuth angles has been inserted for satellites orbiting at low altitudes (1000 km). No correction, however, was introduced for aspect sensitivity in any of the synchronous satellite data or low-altitude satellite data. Many of the observations of the synchronous satellites were compared for magnetiant index sets at one site; the aspect angle did not change. In other cases (Narssarssuaq observations, for example), the angle was large (1240) [at 1800] the ray path and the irregularity are in line] and, therefore, the amplitude is relatively unaffected.

In the case of a site such as Sagamore Hill and observations of either BE-B or Transit 4A, the manner of lumping data along a line of constant latitude (at various aspect angles) has minimized the effect; the dominant term is a latitudinal variation.

In the case of observations of BE-B from Narssarssuaq and at all times from Thule, aspect sensitivity could be an important factor. Since the minimum propagation angle occurs when the line of sight to the saiellite is along the lines of force of the earth's field, in the case of Narssarssuaq and Thule data it is to be expected that minimum index would occur along the magnetic meridian and to the south of the station. At noon from Narssarssuaq (Nielsen and Aarons, 1973), maximum index occurred to the north of the observatory. At all times at Thule, scintillation index occurrence was maximum to the north of Thule in the direction of the corrected geomagnetic pole. A correction, however, should be made to absolute values but the indices given in this paper in the polar cap region are: hardly in that category.

It might be noted that in an analysis of 4° MHz data from BE-B taken in souther a polar regions. Titheridge and Stu. (1.068) found a high level of activity over a region between the southern geographic pole and the geomagnetic pole. From a position almost equidistant from the geographic, they observed the geomagnetic and the dip poles. A similar lumping together of the data supplied by Mullen and Buerkle (private communication, 1971) of the scintillations of the 150 MHz transmissions from the Transit satellite is shown in Figure 1.10. K indices were limited to 0-2. Maximum scintillation occurrence is rear the vicinity of the corrected geomagnetic pole; this is considerably higher than the Foxe Basin maximum found by Penndorf (1962) in his notionside-spread F analysis. Thus it can be seen that aspect sensitivity cannot account for the polar maximum near the geomagnetic pole.

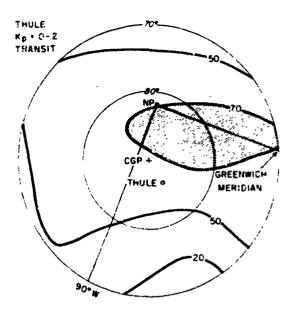


Figure 1.10. Occurence of Scintillations (Arbitrary on-off Determination) at 150 MHz From the Transit Satellite Observed at Thule for Kp = 0-2. All times of day are included in this series of observations during the summer of 1968. Data from Mullen and Buerkle (private communication)

#### L5 DISCUSSION

The morphology and latitudinal variations of F-layer irregularities—as shown by scincillation observations—set limitations to proposed mechanisms for the origin of the irregularities.

Low energy electrons, from 1 to 1000 eV, precipitating into the ionosphere will produce ionization at F-layer heights (Frihagen, 1969). The polar boundary observed for precipitation of electrons of a few hundred electron volts negates the concept that these electrons are sources for production of irregularities. In reviewing high latitude observations of low-energy particle precipitation, O'Brien (1970) found that fluxes in the polar cap (defined for his study as 74° to 34° during local day and 71° to 83° during local night) were 10 to 1000 times less than in the soft zone. Hoffman (1970) cund the polar cavity appearing as a region of no measureable precipitation (with the detectors used). Yet all available data between 750 and the pole (Frihagen, 1971; Titherage and Stuart, 1968; Nielsen and Aarons, 1973) show that a high occurrence of scintillation prevails throughout this region. Maier and Rao (1970), observing suprathermal electrons (> 5 eV), discuss a poleward boundary higher than the - iroral oval. In their graphs, they show less difference between auroral oval flux and polar flux for suprathermal electrons than for the higher energy electrons. R. Sagalyn (private communication, 1973) observing thermal positive ion flux over high latitudes, most often failed to find a poleward boundary for the irregularities observed.

Another possible mechanism is the generation of instabilities at F-layer heights by the precipitation of low energy electrons. The wave motion might then flow roleward and equator and. An important characteristic of scintillation, however, is its great variability within spans of tens to hundreds of kilometers. It would be reasonable to expect waves generated at nigh latitudes in relatively small east-west regions to spread our uniformly at lower latitudes over larger east-west areas. Scintillation characteristics, as shown in Basu et al (1964), show considerable differences between neighboring geographical areas. In addition, it is difficult to account for the stopping of a wave motion abruptly at the scintillation boundary. One characteristic of scintillation—the decrease in irregulacity intensity from the auroral eval to the boundary—would, however, fit in with an attenuation of a wave generated in the auroral eval.

The characteristics of scintillation in the irregularity region point to another possible mechanism; that is, the disturbance of field lines. In their measurements of electric fields at 400 km, Kelley and Mozer (1972) have found variations with tatitude in the boundary region, the auroral oval, and the polar regions which resemble those recorded in scintillation studies. Maximum signals of a turbulent isotropic electric field were found in regions of invariant latitude corresponding to the average position of the oval. High intensities were also found in polar regions. Day values decreased significantly over the geomagnetic price relative to auroral oval levels in their spring measurements. One the hypotheses, advanced by Kelley and Mozer, is that the signals they detect with their experiment are due to electrostatic oscillations established independently on neighboring field lines. This hypothesis would satisfy the observations of localized variations, as well as the need to introduce an ex, lanation of the polar observations of a high occurrence of deep fading.

Although the "tweaking" of magnetic field lines both in the closed and open field lines appears to satisfy observational demands, it hardly explains what produces the change in conductivity along the field lines from closed field lines right into the tail.

#### I.6 A WWARY

The outlines of the intensity variations within the irregularity region are clear. At might during periods of magnetic quiet, scintillation index increases several old from the boundary to the auroral oval latitudes. Maximum index is recorded in the auroral oval region. A shallow minimum is then encountered with a second peak located near the corrected geomagnetic pole. Higher magnetic indices both increase intensity levels across the entire irregularity region, and

lower the boundary between the ordered F layer and the F layer encrusted with small scale irregularities.

The daytime boundary is located between  $71^{\circ}$  and  $76^{\circ}$  for very low K indices (K = 0, 1) and  $68-6^{\circ}$  for K = 2, 3. Increased magnetic activity brings higher levels of scintillations throughout the region from the boundary to the corrected geomagnetic pole during the day, as well as during the night.

Low energy electrons would precipitate at F-layer heights. The normal absence from the polar regions (the polar cavity) of a high flux of electrons greater than several hundred eV, however, makes it difficult to ascribe F-layer irregularities directly to precipitation of electrons within this energy range. Suprathermal electrons (> 5 eV) and thermal electron irregularity patterns, however, show occurrence similar to those of scintillation indices. An association—which is very close from the point of view of latitude of occurrence, variation with magnetic index, and polar pattern—is that of electric field turbulence. One of the two possible reasons for he presence of the isotropic turbulent electric fields put forth by Kelley and Mozer (1972)—that is, the change in conductivity along individual field lines—is thought reasonable from the viewpoint that scintillation characteristics with their strongly localized intensity variations demand localized field line variations.

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## 2. A Graphical Description of Scintillation Occurrence Patterns

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#### 2.1 INTRODUCTION

Utilizing observations of ATS-3 at 136-137 MHz, 15-min scintillation indices were scaled from chart records. The observations for the stations were taken over varying periods of time. From the Sagamore Hill Radio Observatory where the mean intersection latitude was  $\sim 54^{\circ}$  invariant (elevation angle  $\sim 40^{\circ}$ ), the data encompass the period from November 1967 to March 1972 with some gaps in the reduced data base. From the Narssarssuaq Observatory of the Danish Meteorological Institute, the records were reduced for the period September 1968 to March 1972 (with gaps). The mean intersection latitude was  $\sim 64^{\circ}$  with an elevation angle of  $\sim 18^{\circ}$ . The Thule observations made at the AFCRL Geopole Station, through an impresection latitude of  $72^{\circ}$  invariant and an elevation angle of  $\sim 4^{\circ}$ , were reduced for  $\sim 90$  days; it was felt that the wide range of variations and the low angle of elevation limited the utility of the Thule data and therefore the need to reduce more data.

In the graphical (and statistical) analyses, we have utilized seasons to conform approximately with astronomical considerations (February, March, and

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April for Spring, etc.). We have subdivided magnetic index into the three groups: Kp = 0, 1, Kp = 2, 3, and Kp = 4-9. We use K throughout the studies shown. In Appendix A, we use K index groups to assist the systems analyst in organizing the data for applicability to different stages of the sunspot cycle.

#### 2.2 THE SAGAMORE HILL RADIO OBSERVATORY

The data for the Sagamore Hill intersection is that applicable to a subauroral position.

The diurnal pattern for each of the four seasons is summarized for all of the data reduced in Figures 2.1(a), (b), and (c) for the magnetic groupings K = 0, 1, K = 2, 3, and K = 4-9.

For K=0,1, the occurrence of scintillation indices is somewhat higher in the spring than in the other seasons, with winter showing the lowest maximum to minimum ratio. The same pattern takes place when the K indices are higher (2,3); that is, maximum occurrence of indices greater than 20 in the spring and smallest diurnal variation during the winter. The seasonal pattern of high spring values continues in Figure 2.1(c) (K indices are 4-9 while the scintillation in lex is greater than 40 in this case). Winter continues to have a relatively high postnoon level.

Subdividing the data into individual seasons, year by year, the graphs of Figures 2.2(a), (b), (c), and (d) result for K indices of 0, 1. The pattern for each season has some degree of consistency for each of the years shown. Similar graphs for K = 2, 3 are shown in Figures 2.3(a) - (d). The total data bank is used for the K sorts of Figures 2.4(a) and (b).

Using the mean of the occurrence of SI > 20—the two highest hourly values of scintillation index—to characterize individual seasons, Figure 2.5 has been constructed for K = 0-3; the data is inadequate to determine the effect of changing sunspot number. The particular period of time, 1968-1972, had several years of almost identical sunspot number.

#### 2.3 NARSSARSSUAQ, GREENLAND

The seasonal comparison for the Narssarssuaq data is shown in Figures 3, 6(a)-(d). The quiet day curves of K = 0,1 can be noted in Figure 2, 6(a). Summer has the highest maximum of occurrence of scintillation indices greater than 60 (the parameter used in most of the curves in this section) with winter showing a very small change diurnally. This pattern of very high occurrence of deep fading at night in the summer (and to a lesser extent in the spring) also

shows up in K indices of 2,3 [Figure 2.6(b)]. An afternoon maximum is seen in winter with a low occurrence of nighttime scintillations. It might also be noted that summer levels go to zero during early morning hours even when the nightly occurrence is above 90 percent. With magnetic storm conditions, the same diurnal variations hold. In Figure 2.6(c) we continue to use SI > 60, while in Figure 2.6(d) we have plotted SI > 60. It might be noted that minimum occurrence for the  $64^{\circ}$  latitude intersection occurs before noon for all K indices. A post-noon hump can be noted at high K indices in three seasons: winter, fall, and summer.

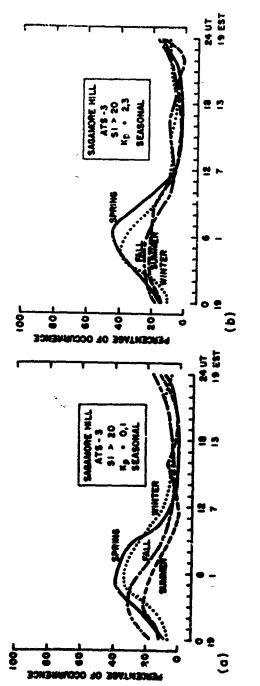
The pattern of occurrence for each season for the years with adequate reduced data is shown in Figures 2.7(a) - (d) for K=0, 1, and Figures 2.8(a) - (d) for K=2,3; it is believed that the data were remarkably consistent when the sorts have been performed in the manner shown. The magnetic storm data have too high values and are too sparse to show the pattern of seasonal behavior year by year.

Figure 2. 9 utilizes the entire data bank to determine the trend of indices. From Figure 2. 9(a), it can be noted that the time of maximum occurrence of SI > 60 shifts towards the latter part of the morning with increasing K index. Figure 2. 6(b) shows the diurnal pattern using the occurrence of very high scintillation index of 80 for K = 9-3, and K = 4-9.

To determine the long term trends of the material, Figure 2.10 has been plotted. The mean of the two highest hourly values of percentage of occurrence of SI > 60 has been plotted (K = 0-3). Little can be said about the effect of the sun; only with the oncoming solar minimum can the effect of solar flux be evaluated.

#### 2.1 THE LE, GREENLAND

Problems with Thule recordings were considerable. Since the angle of elevation was so low  $(\sim 4^{\circ})$  and the wave propagation path almost always through the auroral oval (at some height), scintillations at 136 Milz were very high. Figure 2.11 shows Thule SI > 60 for K = 0, 1 and SI > 80 for K = 0-3. A high percentage of occurrence at night can be noted for what is effectively our highest value of scintillation index (SI > 80).



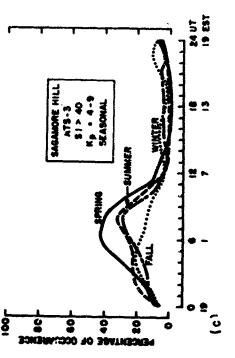


Figure 2.1

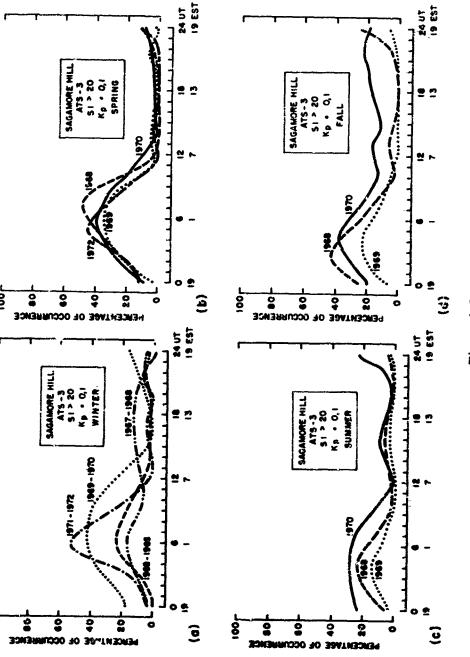


Figure 2, 2

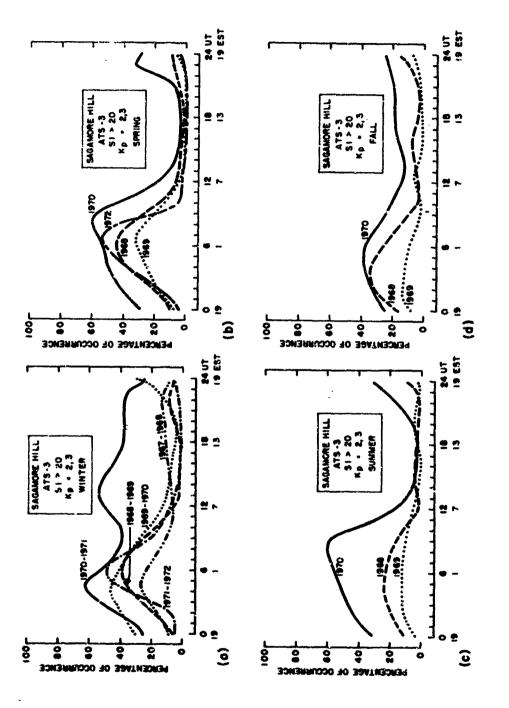


Figure 2.3

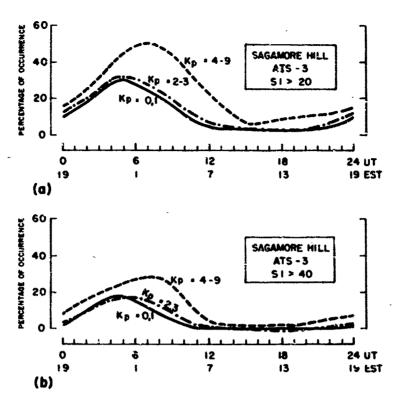


Figure 2.4

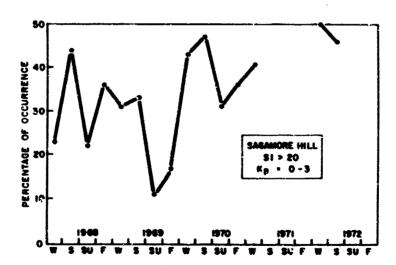
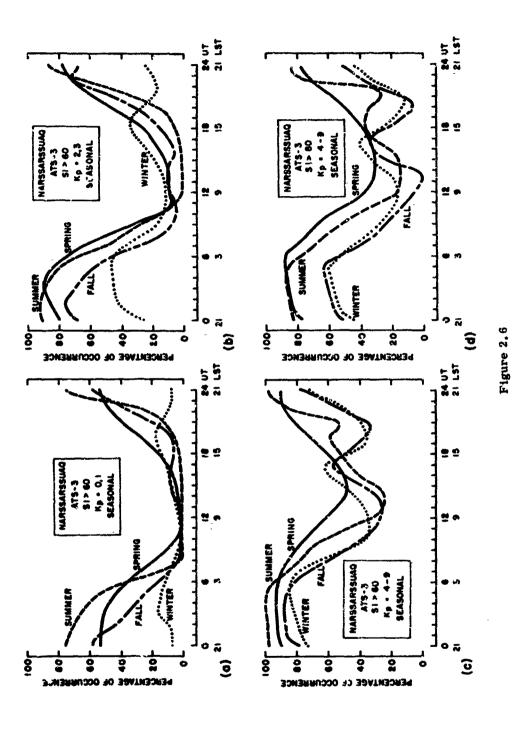


Figure 2.5

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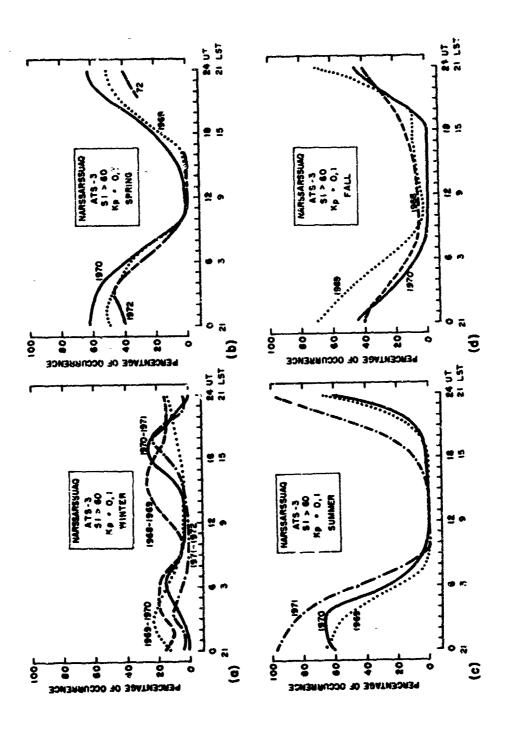


Figure 2.7

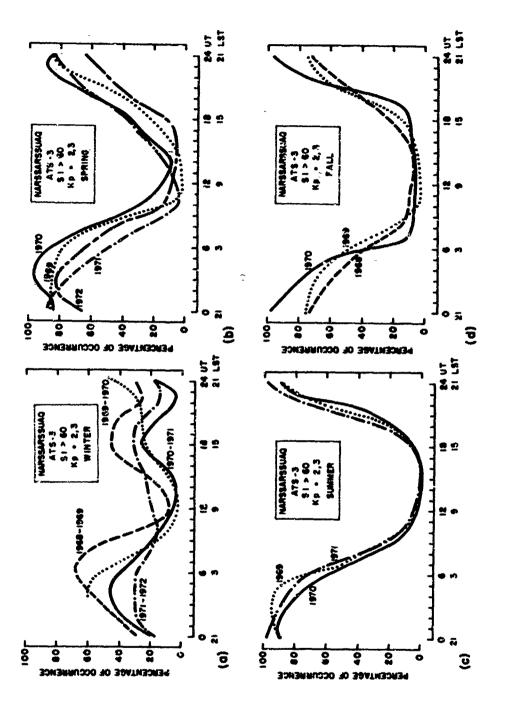
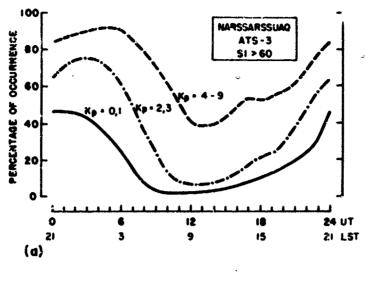


Figure 2.8



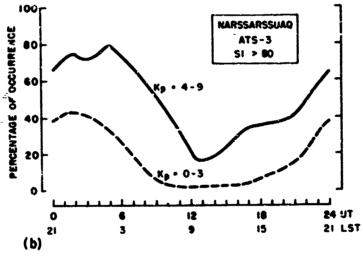


Figure 2.9

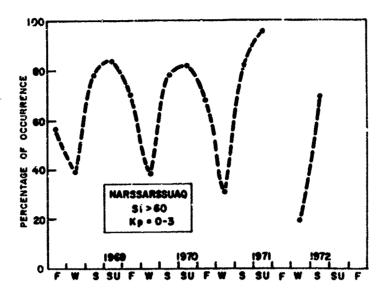


Figure 2.10

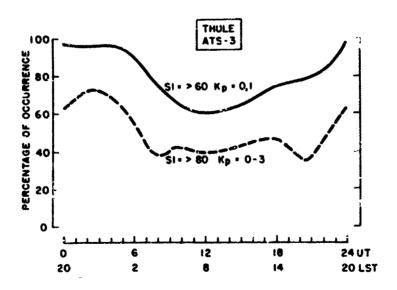


Figure 2.11

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# 3. A High Latitude Statistical Model of Scintillations Using the Cumulative Amplitude Probability Distribution Function

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#### 3.1 INTRODUCTION

Various scintillation indices have been used to describe the depth of amplitude scintillations. These indices can be summarized into four types dependent on whether mean or rms value describes the excursions and whether amplitude or power describes the signals. Briggs and Parkin (1963) and Bischoff and Chytil (1969) list and discuss the indices.

At AFCRL, a standard method of measurement was adopted for ionospheric studies (Whitney et al. 1969). The aim of the studies was to describe the morphology of the irregularity structure. Therefore a simple method had to be utilized to reduce the strip charts. The index adopted is defined as:

S. I. 
$$(\%) = \frac{P_{\text{max}} - P_{\text{min}}}{P_{\text{max}} + P_{\text{min}}} \times 100$$
, (3.1)

where P<sub>max</sub> is the third peak down from the maximum and P<sub>min</sub> is the third minimum up from the lowest excursion in the given sample period. The majority of the data that is to be described was scaled to have one index value which characterized a 15-min interval. The data used is that obtained by observations of various synchronous satellites transmitting at 136 MHz. A 15-min sample interval was chosen in order to achieve stationarity or constancy of scintillation index over the measurement period. In the latitudes just below the auroral oval, scintillations have periods that range from about 1/sec to 1/min with a median value of six fluctuations per minute. The same range of periods holds for the equatorial region, with longer periods observed in the post midnight hours (Aarons et al. 1971). Faster fluctuations are frequently observed at high latitudes, when observing synchronous satellites at low angles of elevation through the auroral oval. Examples of the variation in rate can be seen in the strip chart reproductions in Figure 3.1. A 15-min interval will, therefore, include many periods of the scintillations, while a longer sample interval for the measurement of S.I. would be subject to possible changes in scintillation index from the variability of the propagation path.

#### 3.2 SCINTILLATION INDEX AND PROBABILITY DISTRIBUTIONS

The parameter scintillation index does not describe precisely the fading characteristics of the signal in sufficient detail for either the engineer interested in propagation effects, or for the physicist interested in determining scattering mechanisms for the signal. Engineers designing satellite systems must determine the fading margin necessary to overcome ionospheric scintillations under various conditions—and for a particular electronic configuration. The time percentage that the signal fades below various levels as a function of local time, latitude, season and magnetic index is usually required for a complete evaluation of the expected performance of the proposed systems. The physicist interested in determining the mechanism of scatter or diffraction can wilize the amplitude probability distribution to determine various regimes in which different scattering mechanisms hold. In particular, the distributions will fall into ranges from the strong scattering in the Nakagima q-distribution (approximate Hoyt distribution) through the Rayleigh distribution to the n-weakly scattered distribution (approximate Rice distribution) (Nakagami, 1960; and Bischoff and Chytil, 1969). The model to be shown was developed by converting statistics on scintillation indices to a cumulative amplitude probability distribution function (cdf). The cdf expresses the probability or percentage of time that the signal amplitude will equal or exceed a given amplitude.

## 3.3 SCINTILI ATION INDEX GROUPS AND THEIR CDF WODELS

The scaled values of scintillation index were placed into six groups. Within each group, a range of scintillation indices were encompassed. The groups and ranges of S.I. with their corresponding changes in signal level are shown in Table 3.1.

Groups	Scintillation Index (%)	P <sub>max</sub> -P <sub>min</sub> (dB)
0	< 20	< 1.7
1	20 - 39	1.7 - 3.6
2	40 - 59	3.7 - 5.9
3	60 - 79	6.0 - 9.4
4	80 - 89	9.5 - 12.7
5	≥ 90	≥ 12. 6

Figure 3.1 shows an example of data and the corresponding distribution for each S.1. group. The data for the models were taken utilizing the 150-ft parabola of the Sagamore Hill Radio Observatory. With this antenna, the signals from ATS-3 were recorded at a signal-to-noise ratio of over 30 dB thus insuring sufficient range to record deep negative fades. The output of the receiving system was recorded on magnetic tape. The tape was digitized and the distributions were made by the use of a PDP-9 computer acting as a data processor. Each of the amplitude probability distributions thus obtained for a 15-min segment was then sorted according to the measurement of the simplified scintillation index Eq. (3.1). In order to make each model, many 15-min samples were analyzed in this way. Table 3.2 lists the number of records processed to yield a corresponding median cdf or model distribution.

Table 3.2. Tabulation of Distribution by Groups

S.I. Group	No. of 15-min Distributions
1	49
2	45
3	70
4 .	50
5	110

A total of 324 distributions was obtained with the division between the S. I. groups as listed. From the sample size for each S. I. group, the median distribution was taken as the central value and called a model distribution for that group. Five model distributions are snown in Figure 3.2. The sixth, group 0, was not measured and is assumed in the model to be constant at the median (0 dB) level. Since group 0 does include small scintillations, less than 20 percent, it is realized that there will be some departure from the median (0 dB) for extreme probabilities. It was estimated, however, that this assumption was justified for engineering applications. The dotted lines, which bracket the group 5 model distribution, define  $\pm$  three times the standard error of the mean,  $\sigma_{M} = \frac{\sigma}{\sqrt{N}}$ , where  $\sigma$  is the standard deviation and N is the number of distributions in the group. This confidence interval is a measure of the probable extent to which a model distribution of group 5 is apt to vary with future samplings. The limits defined by  $\pm 3\sigma_{M}$  for the model distributions of the other S. I. groups were comparable to those shown for group 5. The number of samples in group 5 was deliberately made larger than the others to increase accuracy for extreme deviations from the median level,

As will be shown later, the individual 15-min distributions closely followed the Nagakami m-distribution and could therefore be related to a particular value of the m-parameter. Since the individual distributions which comprise each S. I. group agree closely with Nakagami distributions, the median for each group is also a Nakagami distribution. In Figure 3.2 the curves are solid over the range that the median, of the experimentally determined distributions, agreed with a theoretical m-distribution within 0.5 dB. Experimental accuracy was not sufficient to determine the extreme values, and the dotted lines are extended in accordance with the theoretical m-distributions for values of m given in the parenthesis.

The model distributions shown in Figure 3.2 are used in the following manner to determine a cdf which corresponds to the frequency of occurrence of the S.I. groups for a given period. The percent occurrence of each S.I. group is multiplied by its probability at each dB level, as given in Figure 3.2, and the values summed to give a composite curve. Expressed mathematically:

where f(G) is the frequency of occurrence of a group and P(dB) is the probability or percent of time at each dB level from Figure 3.2. Three distributions are shown in Figure 3.3 representing the conversion of occurrence statistics for two years of data for Hamilton, Mass. Daytime and nighttime variations are separated from all hours. It is noted that a weighted combination of Nakagami distributions produces a composite curve which cannot be represented by a Nakagami distribution.

A question naturally arises concerning the validity of determining a cumulativeamplitude-probability-distribution function in the described manner. One method of determining the validity and accuracy of the conversion process is to compare a derived distribution with one that is well known. During the period 25-30 July 1970, several periods of large scintillations were recorded on the 136 MHz signal from ATS-3. The use of the 150-ft antenna for receiving the signal allowed adequate signal-to-noise ratio for measuring the deepest fades. Since the ATS-3 signal is essentially linearly polarized, a circularly polarized feed was used to eliminate the undesirable effects of Faraday rotation. A total of 35,5 hr of scintillations was recorded, digitized, and processed on a computer to determine the cumulative amplitude distribution shown as the solid curve in Figure 3.4. For the same scintillation period, 15-min scintillation indices were scaled and the percent occurrence of the S.I. groups were converted to a cdf using the model distributions of Figure 3.2. The percent occurrence values were multiplied by the percent of time for each S.I. model distribution and the values summed to give the dashed curve on Figure 3.4. The comparison in Figure 3.4 of the derived distribution with the actual distribution, shows that the distributions agree within 0.5 dB for the abscissa range of 0.1 to greater than 99.9. It is felt that this test denonstrates that distributions can be obtained from the modelling process with sufficient accuracy for engineering applications for midlatitude stations.

## 3.4 HIGH LATITUDE CDF

Measurements in the auroral region and at the equator show a considerable increase in the occurrence of deep scintillation over that experienced at midlatitudes. A large data base of S. I. measurements was available from stations in Greenland and Peru. It was proposed that the distribution models (Figure 3.2) determined from Hamilton, Mass. data could also be applied to convert S.I. measurements from other sites to a cdf and thus determine lading margins for other geographical regions. To determine the validity of the conversion technique for other latitudes, the following procedure was used. From the signal-strength records for each of the other sites, cumulative distributions were manually scaled. The solid curve in Figure 3.5 is the distribution for Narssarssuaq, Greenland which was obtained by scaling 10.25 hr of strip charts which displayed a range of scintillations. The solid curve in Figure 3.6 is the distribution for Huancayo, Peru and represents 7 hr of scintillating data. For each of the sets of data, the occurrence of the 15-min S. I. was found as tabulated by groups on Figures 3.5 and 3.6. The occurrence values of the S.I. groups were then converted to a distribution using the models (Figure 3.2) from Hamilton data, and shown as dashed

corves on Figures 3.5 and 3.6. Figure 3.5 for the auroral region shows that the modelling process gives a distribution that compares with the manually obtained distribution within 1 dB for the percentile range of 1 to greater than 99. Comparison of the two distributions in Figure 3.6 for the equatorial region shows a significant departure for percentiles less than 1 and greater than 98. This could be a real effect in that a group 5 model for Peru could give greater changes in amplitude in the extreme percentile ranges; that is, it would be represented by a smaller value of m than was found for Hamilton data, or it could be that the sample size of 7 hr was not large enough for statistical comparison. It is concluded, however, that the tests which have been described have shown that the models of Figure 3 2 can be used to convert archive data in the form of scintillation indices to edits for midlatitude and auroral regions with sufficient accuracy for engineering applications and over a more limited percentile range for the equatorial region.

## 3.5. ENGINEERING USES OF SCINTILLATION INDICES

It should be noted that there are two distinct ways in which the occurrence of the S. I. groups can be utilized.

- (1) A car can be determined in the previously described manner. This would allow a fading margin to be determined to overcome this propagation effect for whatever conditions are represented by the statistical sort of the S. i. values.
- (2) Relate the depth and occurrence of fading to the particular modulation techniques. For certain modulation systems (very high-speed pulse code for example), if the signal fell below threshold for acceptable signal) only a small percentage of a 15-min period, then the entire 15-min period might be useless unless some form of redundancy were used. Therefore, it is important to list the percentage of time each of the scintillation ranges (and therefore model distributions) occurred for each set of magnetic indices. Projected occurrence of magnetic indices will allow the engineer to forecast occurrence of system disruption. In Table 3, 3 we have listed magnetic index variations.

Table 3.3. Percentage of Occurrence of Magnetic Index Sets

Year	K <sub>p</sub> = 0-3	K <sub>p</sub> = 4-9
1950	72,8	27_2
1951	63.5	36.5
1952	64, 2	35.8
1953	75.3	84.7

Table 3.3 (Contd.). Percentage of Occurrence of Magnetic Index Sets

Year         K <sub>p</sub> = 0-3         K <sub>p</sub> = 4-9           1954         85.6         13.4           1955         85.9         14.1           1956         74.7         25.3           1957         72.9         27.1           1958         71.6         28.4           1959         68.5         21.5           1960         67.3         32.7           1961         81.7         18.3           1962         82.2         17.8           1963         82.7         17.3           1964         88.0         12.0           1965         93.3         6.7           1966         88.4         11.6           1967         86.6         13.4           1968         81.9         18.1           1969         87.4         12.6           1973         86.8         13.2           1971         85.4         14.6			
1954       85.6       13.4         1955       85.9       14.1         1956       74.7       25.3         1957       72.9       27.1         1958       71.6       28.4         1959       68.5       21.5         1960       67.3       32.7         1961       81.7       18.3         1962       82.2       17.8         1963       82.7       17.3         1964       88.0       12.0         1965       93.3       6.7         1966       88.4       11.6         1967       86.6       13.4         1968       81.9       18.1         1969       87.4       12.6         1973       86.8       13.2	Year	K <sub>p</sub> = 0-3	K <sub>p</sub> = 4-9
1956       74.7       25.3         1957       72.9       27.1         1958       71.6       28.4         1959       68.5       21.5         1960       67.3       32.7         1961       81.7       18.3         1962       82.2       17.8         1963       82.7       17.3         1964       88.0       12.0         1965       93.3       6.7         1966       88.4       11.6         1967       86.6       13.4         1968       81.9       18.1         1969       87.4       12.6         1973       86.8       13.2	1954	85.6	
1957       72.9       27.1         1958       71.6       28.4         1959       68.5       21.5         1960       67.3       32.7         1961       81.7       18.3         1962       82.2       17.8         1963       82.7       17.3         1964       88.0       12.0         1965       93.3       6.7         1966       88.4       11.6         1967       86.6       13.4         1968       81.9       18.1         1969       87.4       12.6         1973       86.8       13.2	1955	85.9	1 <b>4.</b> î
1958       71.6       28.4         1959       68.5       21.5         1960       67.3       32.7         1961       81.7       18.3         1962       82.2       17.8         1963       82.7       17.3         1964       88.0       12.0         1965       93.3       6.7         1966       88.4       11.6         1967       86.6       13.4         1968       81.9       18.1         1969       87.4       12.6         1973       86.8       13.2	1956	74.7	<b>25.</b> 3 -
1959     68.5     21.5       1960     67.3     32.7       1961     81.7     18.3       1962     82.2     17.8       1963     82.7     17.3       1964     88.0     12.0       1965     93.3     6.7       1966     88.4     11.6       1967     86.6     13.4       1968     81.9     18.1       1969     87.4     12.6       1973     86.8     13.2	1957	72.9	27.1
1960       67.3       32.7         1961       81.7       18.3         1962       82.2       17.8         1963       82.7       17.3         1964       88.0       12.0         1965       93.3       6.7         1966       88.4       11.6         1967       86.6       13.4         1968       81.9       18.1         1969       87.4       12.6         1973       86.8       13.2	- 1958	71.6	28.4
1961     81.7     18.3       1962     82.2     17.8       1963     82.7     17.3       1964     88.0     12.0       1965     93.3     6.7       1966     88.4     11.6       1967     86.6     13.4       1968     81.9     18.1       1969     87.4     12.6       1973     86.8     13.2	1959	68.5	21.5
1962     82. 2     17. 8       1963     82. 7     17. 3       1964     88. 0     12. 0       1965     93. 3     6. 7       1966     88. 4     11. 6       1967     86. 6     13. 4       1968     81. 9     18. 1       1969     87. 4     12. 6       1973     86. 8     13. 2	1960	67.3	32.7
1963     82.7     17.3       1964     88.0     12.0       1965     93.3     6.7       1966     88.4     11.6       1967     86.6     13.4       1968     81.9     18.1       1969     87.4     12.6       1973     86.8     13.2	1961	81.7	18.3
1964     88.0     12.0       1965     93.3     6.7       1966     88.4     11.6       1967     86.6     13.4       1968     81.9     18.1       1969     87.4     12.6       1973     86.8     13.2	1962	82.2	17.8
1965     93.3     6.7       1966     88.4     11.6       1967     86.6     13.4       1968     81.9     18.1       1969     87.4     12.6       1970     86.8     13.2	1963	82.7	17,3
1966       88.4       11.6         1967       86.6       13.4         1968       81.9       18.1         1969       87.4       12.6         1975       86.8       13.2	1964	88.0	12.0
1967     86.6     13.4       1968     81.9     18.1       1969     87.4     12.6       1973     86.8     13.2	1965	93.3	6.7
1968     81.9     18.1       1969     87.4     12.6       1970     86.8     13.2	1966	88.4	11.6
1969     87.4     12.6       1970     86.8     13.2	1967	86.6	13.4
1970 86.8 13.2	1968	81.9	18.1
	1969	87.4	12,6
1971 85.4 14.6	1970	86.8	13.2
	1971	85.4	14.6

## 3.6 THE NAKAGAMI DISTRIBITION

The method described in this report was developed as a means of converting archive data of scintillation indices to a cdf. The tests on the accuracy of the method indicate that it is sufficient for engineering applications, except possibly in the extreme percentiles and for the equatorial region. An analysis of a greater number of 15-min distributions of the group 5 category is necessary for equatorial scintillations to determine if the model of Figure 3.2 will fit that area.

Bischoff and Chytil (1969) showed that an approximate measure of scintillation index, Eq. (3.1) and the exact measures of Briggs and Parkin (1963) were closely related. In their analysis, Bischoff and Chytil have used Nakagami's a distribution as a measure of scintillations. The distribution function of intensity \( (dB) ) is given by:

$$p(X) = \frac{2^{-2^{m}}}{M[\Gamma(m)]} \exp \left[ m \left( \frac{2X}{M} - e^{2X/M} \right) \right]$$
 (3.2)

where  $M = 20 \log_{10} e = 8.686$ . A plot of the cumulative distribution is shown on Figure 3.7, for several values of m from 1 to 40. Even though only integer values are shown, m is continuously variable and can have any value  $\geq 0.5$ . It is also evident that the fading range is proportional to 1/m.

Six experimental 15-min distributions from group 5 and four distributions from group 4 are plotted in Figure 3.8. The two solid curves are the theoretical distributions with m = 1 and 1.3 and the dashed curve is m = 4. No test of fitness was made, but, since m can have other closely spaced values to those shown, visual inspection leads to the conclusion that there is good agreement between the theoretical curves and the experimental distributions.

Experimentally obtained distributions from S. I. g. cups 3, 2, and 1 have been found to agree with theoretical distributions having m values ranging from 6 through 100. Since the 15-min distributions agree very closely with the theoretical m distributions over the measurement range, extreme values can be approximated from the theoretical curves when required. For example, a fade depth of -27 dB is indicated for the 99.9 percentile for the m = 1 distribution.

## 3.7 FREQUENCY DEPENDENCE

The frequency of a system in the design study phase can be a variable with the choice at times within only a short range (225 MHz to 400 MHz, for example) or between frequencies differing by an order of magnitude (136 MHz to 1550 MHz). With available data the tradeoffs possible can be evaluated at middle and high latit des in the first case with a fair degree of certainty.

'The frequency dependence can be determined by relating the ratio of the amount of power in the scintillating component to the frequency ratio. Aarons et al. (1967) determined the frequency dependence of radio star scintillations from the relationship:

$$\eta = \log \frac{S_1}{S_2} / \log \frac{f_1}{f_2}$$
(3.3)

where S is the scintillation index of Eq. (3.1).  $\eta$  is termed the spectral index of the scintillations. This expression is valid as long as S is a constant power law function of frequency. A log-log plot of S vs f will result in a straight line with a slope equal to  $\eta$ . Their results show that the scintillation index is inversely proportional to frequency squared for weak scintillations, and approaches a 1/f dependence for high levels of scintillation. As pointed out earlier, however, scintillation index is not a convenient system design or physical parameter.

It has been shown (Chytil, 1967) that:

$$S_A = \sqrt{1/m} \text{ for } m \ge 0.5$$
 (3.4)

where  $S_4$  is the notation used by Briggs and Parkin (1963) to measure the scintillation depth as the root-mean-square power deviation divided by the mean power, and m is Nakagami's parameter.

By substituting  $\sqrt{1/m}$  for S in Eq. (3.3), it can be found that:

$$-2 \eta = \log \frac{m_1}{m_2} / \log \frac{f_1}{f_2} = \eta_m . \tag{3.5}$$

If  $\eta_m$  can be evaluated from simultaneous distributions for two frequencies from the same source, then prediction of the expected distribution at a desired frequency can be made as long as scintillation index and m remain a constant power of frequency.

The technique is illustrated in Figure 3.9 which shows the experimentally determined cdf's for two frequencies. By comparing the experimental distributions while theoretical distributions, it can be seen that these distributions approximately follow a theoretical distribution of m = 1.5 for 137 MHz and m = 40 for 412 MHz. Evaluation of  $\eta_{-}$  gives:

$$\eta_{\rm m} = \log \frac{1.5}{40} / \log \frac{137}{412} = 2.98$$
 (3.6)

[ From Eq. (3.5) this value of  $\eta_m$  would correspond to a scintillation index spectral law of -1.5]. Using the value of  $\eta_m$  from Eq. (3.6) and assuming that a constant power law relationship holds over the frequency interval, a predicted distribution with m = 9.5 would be obtained at 254 MHz.

If strong—attering is observed, that is,  $0.5 \le m \le 1$  on the lower frequency, a constant power, law relationship may not be the case and interpolation or extrapolation for a distribution at other frequencies may be untenable.

To determine the spread in experimentally determined values of spectral index  $\eta_m$ , 22 simultaneous records of scintillations at 137 and 412 MHz were processed to give corresponding 15-min cumulative amplitude distributions. The values of  $\pi$  varied from 1.1 to 4.9 at the lower frequency and from 24 to 100 at the higher frequency. Spectral indices were calculated from the values of  $\pi$  and frequency of occurrence is shown in Figure 3.10. The data peaks in the range of 2.8 to 3.1.

#### 3.8 ANGLE OF ELEVATION EFFECTS

The basic formula for describing the effect of angle of elevation on scintillation is given by Briggs and Parkin (1963):

$$S_{2\lambda} (\text{sec i})^{1/2} \left\{ 1 + \frac{\pi^2 L_c^4}{4\lambda^2 Z^2} \right\}^{-1/2}$$

The difficulty in testing the equation is that in practical situations, the propagation path to two synchronous satellites traverses two differing invariant latitudes. For a short period (15 January to 15 April 1968) simultaneous data from ATS-3 and Canary Bird were compared utilizing the cdf technique. Figure 3.11(a) graphs the results of a comparison for one satellite, Canary Bird, at approximately 11° of elevation with that of ATS-3 at 37° of elevation. The graph in Figure 3.11(b) is obtained by plotting the corresponding dB levels for the same percentage of time from Figure 3.11(a) for the two satellites. The slope of the latter curve is 1.28.

The intersection latitude of the two paths differed somewhat. This, coupled with the necessity of placing measurements into their proper context as to falling within near or far field considerations (Aarons et al, 1971), does not allow us to generalize further on angle of elevation effects. The observations approximate theoretical values but are too meager to be definitive.

## 3.9 SUNSPOT NUMBER AND MAGNETIC INDEX OCCURRENCE

A parameter of obvious importance in geophysics is the solar flux or sunspot number. It has been shown that years of high sunspot number show an increase in mean scintillation index relative to years of low sunspot number (Lansinger and Fremouw, 1967). A comparison of measurements for the effect of sunspot number must, however, normalize for the occurrence of magnetic index values. Years of high sunspot number bring a high occurrence of magnetic storms. Greater scintillation activity may be the result of more magnetic storms. Aarons et al (1964) have shown that during magnetically quiet periods (K = 0, 1, 2), increasing sunspot number increases scint llation index but it is of lesser importance than magnetic index.

The data base on which the present statistical study rests is not long enough in time to allow a sunspot number parameter to emerge as a variable. A separation of the cdf's as a function of K groupings, however, has been made. The projected occurrence of K indices can then be utilized to evaluate scintillations for a particular year. In Table 3.3, we gave the occurrence of Kp from 1950 to 1971. In Figure 3.12

we have graphed the occurrence of Kp = 0, 1 and Kp 4-9. It is clear from the table and the graph that the occurrence pattern of quiet and disturbed magnetic indices differ significantly from the sunspot number of 10-cm solar flux parameters.

The data base used for the observations listed in Appendix A are predominantly from 1968, 1969, and 1970.

#### 3.16 DILRNAL AND SEASONAL DEPENDENCE

The descriptive model of the irregularity region indicates it is possible to characterize a geomagnetic latitude by the occurrence of scintillation index groups. The occurrence of scintillations at one location is a function of:

- (i) Local prepagation path intersection time (more properly corrected geomagnetic time).
  - (2) Season.
  - (3) Planetary or local magnetic index.

In this statistical model of fading occurrence, we treat only three latitudes. The first is that of the propagation path from Sogamore Hill through an invariant latitude of 54° (at 350 km altitude). The second is that of a path through a latitude of 64° (Narssarssuaq) and the third through 72° (Thule). The typical angle of elevation to ATS-3, the source used for this data, was 40° for Sagamore Hill, 18° for Narssarssuaq, and 4° for Thule. The synchronous satellite was near its maximum elevation angle for this study (the satellite was positioned near station longitude for two of the observatories for a large portion of the period of data taking). The data has not been normalized for angle of elevation effects; without normalization it is fe't that the data represents a practical situation for the three latitudes.

in Appendix A, the percentage of occurrence of scintillation indices are listed for hourly groupings of local time, seasons, and magnetic index sets. We have also transformed these into cumulative amplitude probability tables.

It is hoped that the tables will be of use in evaluating the effect of scintillations on proposed systems involving high latitude propagation paths from satellites.

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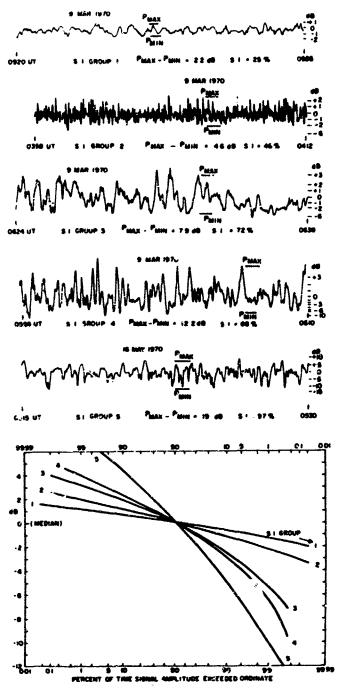


Figure 3.1. Examples of Scintillation Data for Each of the Five S. I. Groups and the Resulting Cumulative Amplitude Pubability Distribution Functions (cdf). Fecords were obtained from ATS-3 transmissions at 136 MHz

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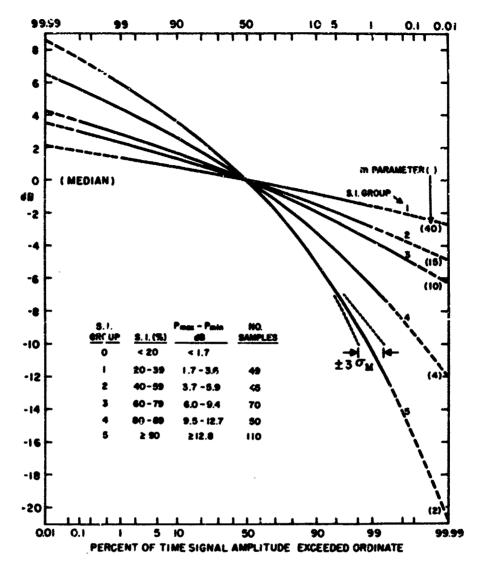


Figure 3.2. Median (Model) Distributions Obtained From the Sample Size for Each S. I. Group From ATS-3 Data Recorded at Hamilton, Mass. Solid curves denote the range of the experimental data; dashed curves denote an extension based on the Nakagami distribution for the value of  $\kappa$  in parentheses.  $\sigma_{\rm M}$  equals standard error of the mean

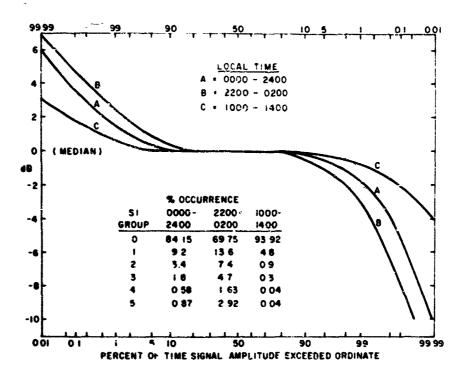


Figure 3.3. Cumulative Distributions for Approximately Two Years of ATS-3 Data at 136 MHz From Hamilton, Mass. These were obtained by the conversion of occurrence statistics of semillation indices (K=0.4) and the use of the distributions in Figure 3.2. The day-te-night variation is shown

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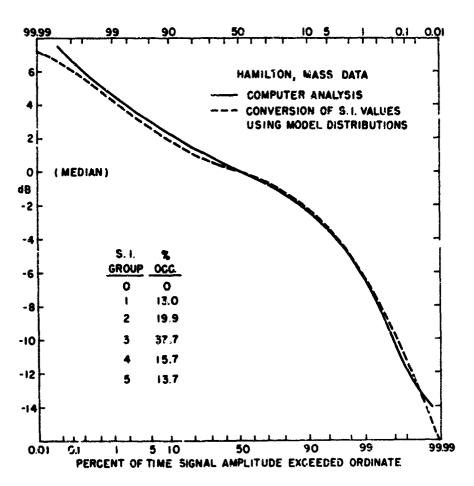


Figure 3.4. Comparison of an Actual Distribution for 35.5 hr of Data (136 MHz) Obtained by Computer Analysis With the Distribution Obtained by the Conversion of the Occurrence of S. I. Groups for the Same Period

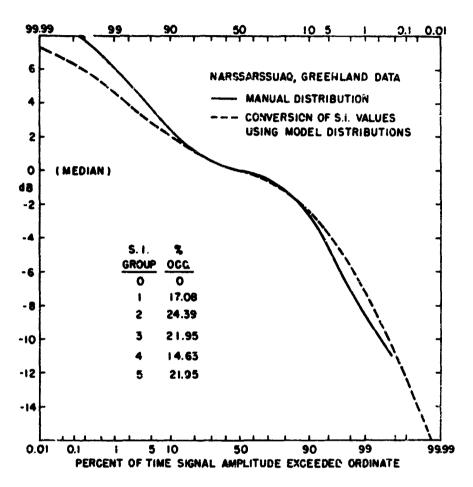


Figure 3.5. Comparison of an Actual D'stribution for 10.25 hr of Data (136 MHz) Taken at Narssarssuaq, Greenland, With the Distribution Obtained From the Hamilton, Mass. Models for the Same Period

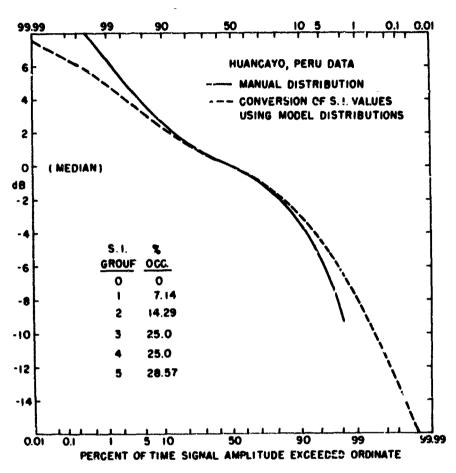


Figure 3.6. Comparison of an Actual Distribution for 7 hr of Data (136 MHz) Taker at Huancayo, Peru, V ith the Distribution Obtained From the Hamilton, Mass. Models for the Same Period

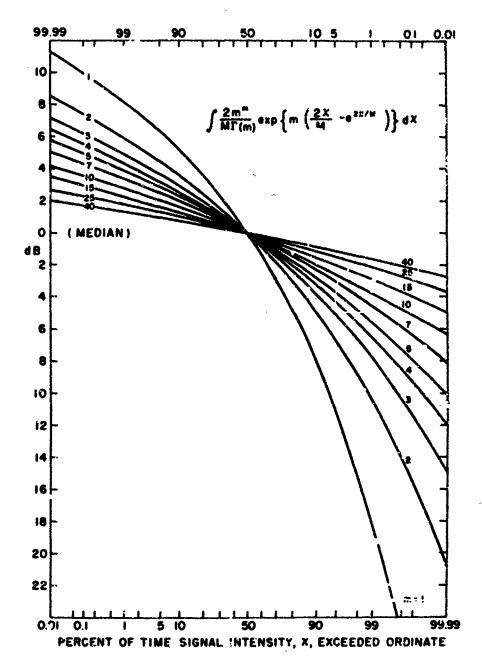


Figure 3.7. Cumulative Form of the Nakagami Distribution: Valid for  $\ge 0.5$ 

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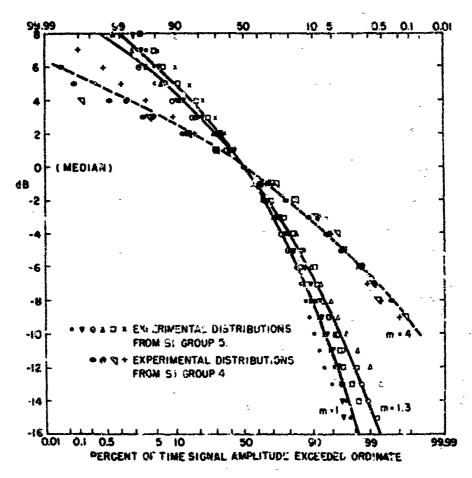


Figure 3.8. Comparison of Theoretical m-Distributions (Solid Line for m = 1 and 1.2 Dashed for m = 4) With Experimental Distributions Fro 3.1. Groups 6 and 5

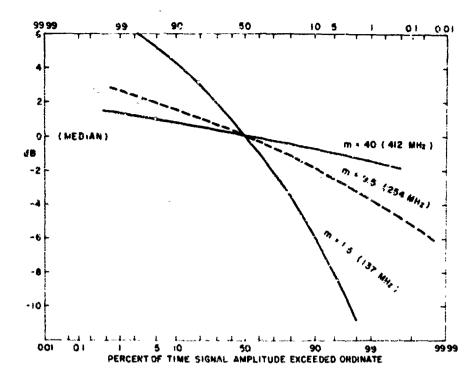


Figure 3.9. The Solid Lines Are the Experimentally Measured Distributions for Simultaneous Recordings of ATS-3 data. The dashed line is an estimated distribution for 254 BHz which was arrived at by interpolating the measurements with the spectral index,  $n_{\pi}$ , as follows:

$$\eta_m = \log \frac{m_1}{m_2} / \log \frac{f_1}{f_2} = 2.98$$

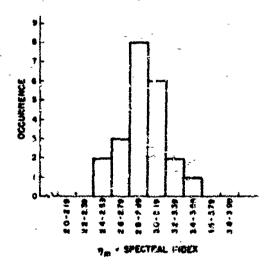


Figure 3-16. Occurrence of Spectral Index Values From a Data Base of 22 Pairs of 15 Min Amplitude Distributions of 137 and 412 MHz Signals where:

$$n_m = \log \frac{m_1}{m_2} / \log \frac{f_1}{f_2}$$

» = Nakagami's Distribution Parameter, and

1 - Frequency

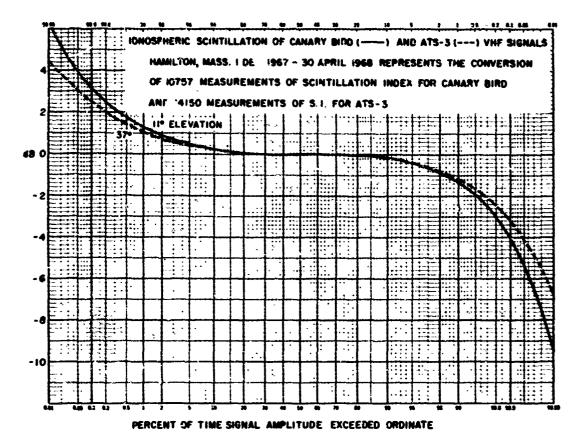


Figure 3 11a. Percent of Time Signal Amplitude Exceeded Ordinate

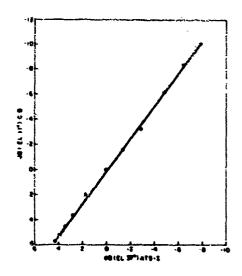


Figure 3-11b. Comparison of Amplitude Probabilities for the Two Paths. Slope is 1,28

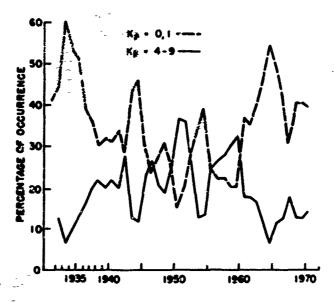


Figure 3. A.J. Variation of Occurrence of Very Quiet Magnetic Indices (K<sub>p</sub> = 0, 1) and Disturbed Indices (K<sub>p</sub> = 4-9) through 1971

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# Appendix A

Cumulative Amplitude Probability Distributions

The following data pages contain analyzed cdf's for the three sites used in the test. Seasonal patterns are shown as well as cdf's for all the data available. Thule seasonal patterns are not given since the data base was judged inadequate.

In the cdf's, the symbol A is placed alongside values where the accuracy of the interpolation routine is doubtful; the symbol B is placed alongside values where the data is extrapolated and also may be doubtful.

	ON ATS-3		NGV-JA	N	1969-72	LGCA	L TIME
X=0-3			NAL VARIA				
	00-24				22-02	02-06	86-18
SI	PCT	PCT	PCT	PCT	PCT	PCT	PCT
JD-19		95.36	90.95	86.93		71.42	90.18
	11.08 3.78	3.46 1.36	8.32 .60	9.38 2.22	18.76 11.19	18.50 6.25	8.02 1.60
60-79	1.42	.18	.09	.93	4.68	2.55	.17
80-89	.28	0.00	.64	.27	.54	.43	8.00
93-99	.51	0.06	0.00	.27	1.56	.45	.84
	86-24	CIUR 10-14	NAL VARII 14-16	TICN 18-22	22-02	02-96	86-19
PCT	DB X		DB X	08	x CB x		
.05	4.51	2.15	2.22	3.46	6.54	5.21	2.53
-10	3.65	1.76	1.84	3.07	5.42 4.41	4.29	2.08
•50	2.83	1.39	1.51	2.37	4.41	3.43	1.68
•50	1.94	. 35	1.12	1.61	3.25	2.42	
1.00	1.41	.56 .42 .17 .35	. 87	1.17	2.41 1.72	1.80	.94
2.00	• 99	• 4 2	• 66	.44	1.82	1.29 .77	•68
5.00 19.00	• 27	. 36	26		1.06	.49	.41 .25
29.00	.16	* B1	.12	.15	.26	.25	.12
30.00	.08	.35 91 .31	.06	.15	.61 .29 .13	.10	.05
48.00	.01	.90	- 52	.01	.05	-04	
50.00	0.00	.90 36.0	.06 .02 0.00	0.88	.05 0.00	.04 0.00	0.80
68-80	. 86	. 12	46		34	83	86
76.00	.01	.13	.05	.83	19	86	.45
69.00	.01 04 22 52	.31 A .30 A .14 A	.05	-09 13 36 87	24	.04 0.08 63 06 16 43 62 -1.50	. 84
90.00	22	.30 A	64 A	13	61	43	86 A
95.00	~•52	-14 8	23	-, 35	-1.12 -2.08	82	26
98.90	-1.09	36	59	-4 76	-2.48	~1.50	65 -1.83
59.10 99.51	· 1.65	-4.35	92 -1.33	-1.35 -1.92	-2.19	-2.12 -2.£2	-1.46
99.80	· 1.65 -2.27 -3.35	-1.55	-1.33 -1.88	-2.78	+5.56	-4.89	-2.06
99.96	-4.35	-2.12	-2.39	-3.67	-7.48	-6.7A	-2.51
99.95	-5.73	61 -1.35 -1.55 -2.12 -2.59	-2.70	-3.67 -4.65	-9.27	-7.04	-3,84
HAHILT	ON 475-3						AL TIME
HAMILT K=0-3	ON 475-3		FEB-A	PR	1969-72		AL TIME
	ON 475-3	CIUF	FEB-A Inal Vari	PR Ation	1969-72	LCC	
<b>K</b> ≈0-3	ON 415-3	CIUF 10-14	FEB-A INAL VARI 14-16	PR ATION 16-22	1 <b>96</b> 9-72 22 <b>-8</b> 2	02-66	06-18
	ON 415-3 09-24 PCT	CIUF 10-14 PCT	FEB-A INAL VARI 14-18 PCT	PR ATION 16-22 PCT	1969-72 22-82 PCT	82-66 PCT	06-18 PCT
K=0-3	ON ATS-3 19-24 PCT 84.63	CIUF 10-14 PCT 96.98	FEB-A NAL VARI 14-16 PCT 97-29 2-56	PR ATION 16-22	1969-72 22-82 PCT	82-66 PCT 78.86	06-18
SI 08-19 20-39 48-59	09-24 PCT 84.63 7.49 3.32	CIUF 10-14 PCT 96.98 2.58	FEB-A NAL VARI 14-16 PCT 97-29 2-56	PR ATION 16-22 PCT 84.78	1969-72 22-82 PCT 64.34	82-66 PCT	06-18 PCT 94.86
SI 08-19 20-39 48-59 60-79	09-24 PCT 84.63 7.49 3.32 2.34	CIUF 10-14 PCT 96.98 2.58 .15	FEB-A INAL VARI 14-16 PCT 97.29 2.56 .10	PR ATION 16-22 PCT 84.78 9.22 2.59	22-82 PCT 64.34 12.52 6.35 6.58	## LCC ### ### ### ### ################	06-18 PCT 94.86 5.83
SI 08-19 20-39 48-59 60-79 80-89	09-24 PCT 84.63 7.49 3.32 2.34	CIUR 10-14 PCT 96.98 2.56 .15 0.10	FEB-A: INAL VARI 14-18 PCT 97.29 2.56 .10 .65	PR ATION 16-22 PCT 84.74 9.22 2.59 1.71	22-82 PCT 64.34 12.52 8.35 8.35 2.41	LCG #2-66 #CT 78.86 12.68 7.98 5.30 1.64	86-18 PCT 94.86 5.83 .66 .19
SI 08-19 20-39 48-59 60-79	09-24 PCT 84.63 7.49 3.32 2.34	CIUF 10-14 PCT 96.98 2.58 .15	FEB-A INAL VARI 14-16 PCT 97.29 2.56 .10	PR ATION 16-22 PCT 84.78 9.22 2.59	22-82 PCT 64.34 12.52 6.35 6.58	## LCC ### ### ### ### ################	06-18 PCT 94.86 5.83 .66
SI 08-19 20-39 48-59 60-79 80-89	09-24 PCT 84.63 7.49 3.32 2.34	CIUF 10-14 PCT 96.98 2.56 .15 0.10	FEB-A: INAL VARI 14-18 PCT 97.29 2.56 .10 .65	PR 4TION 16-22 PCT 84.74 9.22 2.59 1.71 .93	22-82 PCT 64.34 12.52 8.35 8.35 2.41	LCG #2-66 #CT 78.86 12.68 7.98 5.30 1.64	86-18 PCT 94.86 5.83 .66 .19
K=0-3 SI 08-19 20-39 48-59 60-79 80-89 90-99	09-24 PCT 84.63 7.49 3.32 2.34 .87 1.35	CIUR 10-14 PCT 96.98 2.58 .15 0.30 .19 1.36	FEB-AI INAL VARI 14-18 PCT 97-29 2-56 -10 -65 0-00 8-68	PR ATION 16-22 PCT 84.74 9.22 2.59 1.71 .93 .78 ATION 18-22	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.20	82-66 PCT 78.86 12.68 7.98 5.3% 1.64 1.35	96-18 PCT 94-86 5-83 -66 -19 -85 8-88
K=0-3 SI 00-19 20-39 40-59 60-79 90-99	09-24 PCT 84.63 7.49 3.32 2.34 .87 1.35	CIUR 10-14 PCT 96.98 2.58 .15 0.19 1.19 1.36 CIUR 10-14 D6 X	FEB-A: INAL VARI 14-16 PCT 97.29 2.56 .05 0.00 0.68 INAL VARI 14-16 DB X	PR ATION 16-22 PCT 84.74 9.22 2.59 1.71 .73 .78 ATION 18-22 DB	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.00 22-02 X DB X	### CCC  ##############################	06-18 PCT 94-86 5-83 -66 -19 -95 9-90
K=0-3 SI 08-19 20-39 48-59 60-79 80-89 90-99	ON ATS-3 09-24 PCT 84.63 7.49 3.32 2.34 1.35 00-24 X	CIUR 10-14 PCT 96.98 2.58 .15 0.19 7.16 CIUR 10-14 D6 X	FEB-A: INAL VARI 14-16 PCT 97.29 2.56 .10 .05 0.00 0.00 INAL VARI 14-16 03 X	PR ATION 16-22 PCT 84.74 9,22 2.59 1.71 93 978 ATION 18-22 DB 5.23	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.80 22-02 X DB X	## LCC ### ### ### ### ### ### #### ###	06-18 PCT 94-86 5-83 -66 -19 -85 8-88
K=0-3 SI 08-19 20-39 48-59 60-79 80-89 98-99	00 ATS-3 00-24 PCT 84.63 7.49 3.32 2.34 .87 1.35 00-24 DB X 5.96	CIUR 10-14 PCT 96.98 2.50 .15 0.10 .19 7.16 CIUR 10-14 DB X 1.98	FEB-A: INAL VARI 14-18 PCT 97.29 2.56 .10 .05 0.00 8.60 WAL VARI 14-18 03 1.56	PR ATION 16-22 PCT 84.78 9.22 2.59 1.71 .93 .78 ATION 18-22 08 5.23	22-82 PCT 64-34 12-52 8-35 6-58 2-41 5-20 22-82 X Da X 7-85 7-87	## LCC ### ### #########################	86-18 PCT 94.86 5.83 .66 .19 .85 8.88
X=0-3 SI 08-19 20-39 40-59 60-89 98-99 PCT .05	00 ATS-3 00-24 PCT 84.63 7.49 3.32 2.34 .87 1.35 00-24 DB X 5.94 4.86 3.91	CIUR 10-14 PCT 96.98 2.58 .15 0.10 .19 1.19 CIUR 10-14 DB X 1.98 1.98	FEB-AI 14-18 PCT 97-29 2-56 -10 -65 0-00 8-68 NAL VARI 14-18 03 X 1-56 1-26 1-31	PR ATION 16-22 PCT 84.78 9.22 2.59 1.71 .93 .78 ATION 18-22 DB 5.23 4.28 3.35	22-92 PCT 64-34 12-52 8-35 6-58 2-41 5-20 22-92 X Da X 7-85 7-87 5-96	82-66 PCT 78.86 12.68 7.98 5.34 1.64 1.57	86-18 PCT 94.86 5.83 .66 .19 .85 8.88 80-18 DB X 2.19 1.78 1.42
X = 0 - 3 SI 9 20 - 39 40 - 59 60 - 89 90 - 99 PCT - 05 - 10 - 20 - 50	0N 475-3 09-24 PCT 84.63 7.49 3.32 2.34 1.35 00-24	CIUR 10-14 PCT 96.98 2.58 .15 0.19 1.19 1.19 10-14 DB X 1.98 1.98 1.30	FEB-A: INAL VARI 14-18 PCT 97.29 2.56 .105 0.00 0.68 INAL VARI 10-18 1.56 1.26 1.21	PR  ATION  16-22 PCT  84.74 9,22 2.59 1.71 .78 .78  ATION  18-22 DB 5.23 4.26 3.35 2.22	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.00 22-02 X DB X 7.85 7.97 5.96 4.54	82-66 PCT 78.86 12.68 7.98 5.34 1.59 82-86 08 X 6.34 5.23 4.32 3.15	96-18 PCT 94-86 5-83 -66 -19 -95 8-98 8-98 8-19 1-78 1-42 1-81
X=0-3 SI 08-19 20-39 40-59 60-89 98-99 PCT .05	00 ATS-3 00-24 PCT 84.63 7.49 3.32 2.34 .87 1.35 00-24 DB X 5.94 4.86 3.91	CIUR 10-14 PCT 96.98 2.58 .15 0.10 .19 1.19 CIUR 10-14 DB X 1.98 1.98	FEB-A: INAL VARI 14-18 PCT 97.29 2.56 .105 0.00 0.60 INAL VARI 14-18 X 1.56 1.26 1.01 .53	PR ATION 16-22 PCT 84.74 9,22 2.59 1.71 .78 .78 ATION 18-22 08 5.23 4.28 3.35 2.22	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.20 22-82 X Da X 7.87 5.96 4.54 3.52	12-66 PCT 78-86 12-68 7-98 5-34 1-5- 10-86 08 x 5-23 4-32 3-15 2-36	06-18 PCT 94.86 5.83 .66 .19 .05 8.00 8G-18 DB X 2.19 1.74 1.42 1.42
X = 0 - 3 SI 00 - 19 20 - 39 40 - 59 60 - 89 90 - 99 PCT	ON ATS-3 09-24 PCT 84.63 7.49 3.32 2.37 1:35 00-24 X 5.94 4.86 3.91 2.62 1.79	CIUR 10-14 PCT 96.98 2.58 .15 0.19 7.16 CIUR 10-14 X 1.98 1.98 1.98	FEB-A: INAL VARI 14-18 PCT 97.29 2.56 .105 0.00 0.68 INAL VARI 10-18 1.56 1.26 1.21	PR  ATION  16-22 PCT  84.74 9,22 2.59 1.71 .78 .78  ATION  18-22 DB 5.23 4.26 3.35 2.22	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.00 22-02 X DB X 7.85 7.97 5.96 4.54	82-66 PCT 78.86 12.68 7.98 5.34 1.59 82-86 08 X 6.34 5.23 4.32 3.15	96-18 PCT 94-86 5-83 -66 -19 -95 8-98 8-98 8-19 1-78 1-42 1-81
X = 0 - 3 SI 19 20 - 39 40 - 79 50 - 89 PCT 50 1.00 2.00 1.00	ON ATS-3 09-24 PCT 84.63 7.49 3.32 .07 1.35 00-24 X 4.86 3.62 1.79 1.150 .19	CIUR 10-14 PCT 96.98 2.56 .15 0.10 1.19 1.19 1.19 1.19 1.19 1.19 1.19	FEB-A: INAL VARI 14-18 97.29 2.56 0.00 0.68 INAL VARI 14-18 03.56 1.26 1.21 .53 .32 .12	PR ATION 16-22 PC-17 9-22 2.59 1.71 93 -78 ATION 18-22 08 5.23 4.28 3.28 1.98 -24	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.00 22-82 X 7.85 7.96 4.54 3.52 2.42 2.42 2.42	02-66 PCT 78.86 12.68 7.98 5.34 1.64 1.57 02-86 08 X 5.23 4.32 3.15 2.36 1.66 1.66	06-18 PCT 94.86 5.83 .66 .19 .85 8.88 0G-18 DB x 2.19 1.74 1.42 1.81 .74
X = 0 - 3 SI 19 20 - 39 40 - 79 60 - 89 90 - 99 PCT 50 100 20 100 20 100 20 20 20 20 20 20 20 20 20 20 20 20 2	ON ATS-3 09-24 PCT 84.63 7.49 2.37 1.35 00-24 X 5.94 4.86 3.91 2.62 1.79 1.50 1.50 1.92	CIUM 10-14 PCT 96.98 2.56 .15 0.19 1.36 UR 10-14 X 1.30 1.30 1.30 2.37 .42 .43 .43 .43 .43 .43	FEB-A: NAL-18 14-18 97.29 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	PR ATION 16-22 PC.7a 9.22 2.59 1.71 .73 .78 ATION 18-22 08 5.23 4.28 3.32 1.54 1.88 .49	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.00 22-02 X 7.85 7.87 7.97 5.96 4.54 3.52 2.46 1.29 .28	82-66 PCT 78.86 12.68 7.98 5.34 1.57 82-86 08 x 5.23 4.32 3.15 2.36 1.66 .51	06-18 PCT 94.86 5.83 .66 .19 .05 8.00 86-10 DB x 2.19 1.78 1.42 1.42 1.42 1.42 1.42
X = 0 - 3 SI 19 20 - 39 40 - 79 80 - 99 P CTS 100 200 100 100 100 100 100 100	ON ATS-3  09 - 24  90 - 24  84.63  7.49  2.37  1.35  00 - 24  X  4.86  3.96  2.67  1.13  00 - 192  00 - 192  00 - 192  00 - 192  00 - 192	CIUR 10-14 PCT 96.98 2.56 .15 0.19 1.19 10-14 x 1.98 1.30 1.12 .57 .42 .29 .29 .13 .13 .13 .13	FEB-A: INAL -18 14-18 97.29 2.56 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	PR ATION 16-22 PCT: 84:78 9:22 2.59 1.71 978 ATION 22 08 5.23 4.28 3.35 2.25 1.88 49 .24	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.20 22-8 x 7.87 5.96 4.52 2.46 1.63 .28	82-86 PCT 78.86 12.68 7.48 5.38 1.64 1.57 82-86 08 x 5.23 4.32 3.15 2.26 1.66 .51	06-18 PCT 94.86 5.83 .66 .19 .85 8.80 8G-18 DB x 2.19 1.74 1.42 1.42 1.42 1.42 1.42
X = 0 - 3	ON 475-3 99-24 99-24 84-63 99-24 84-63 99-24 84-39 1	CIUR 10-14 PCT 96.98 2.56 0.15 0.19 1.19 10-14 X 10-14 X 1.30 1.12 1.30 1.12 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30	FEB-A: NAL 14-18 14-18 97.29 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	PR ATION 16-22 PCT 04,22 2.59 1.71 .93 .78 ATION 22 DB 23 4.28 3.35 2.22 1.98 .49 .24 .83 -81	1969-72 22-82 PCT 612-52 8-35 6-58 2-11 5-20 22-8 X 7-97 5-96 4-52 1-29 -28 -85 -85	82-66 PCT 78.86 12.68 12.68 1.64 1.57 82-86 08 x 6.34 5.23 4.32 3.15 2.36 1.66 1.66 1.97	06-18 PCT 94.86 5.83 .66 .19 .85 8.88 06-18 08 x 2.19 1.74 1.42 1.81 .74 .52 .29 .16
X = 0 - 3 9 - 3 9 9 - 3 9 9 - 7 9 9 0 - 9 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ON 475-3 99-24 99-27 84-492 84-492 1 - 33 1 - 35 90-5 90-5 90-7 1 - 159 1 - 159 1 - 159 1 - 102 1	CIUR 10-14 PCT 96.98 2.56 3.15 0.19 1.19 10-14 X 10-14	FEB - A I	PR ATION 16-22 PC-78 9,22 2.59 1.71 84.78 78 ATION 22 08 5.23 4.25 2.22 1.54 1.00 -24 -03 -03 -08	22-07 22-07 64.52-6.34 12.53-6.34 5.420 2-0 5 2-0 5 2-0 5 2-0 5 2-0 5 3.54-22 4.55-42 1.63 -62 -62 -62 -62 -62 -62 -62 -62 -62	02-66 PCT 78.86 12.68 7.98 5.30 1.64 1.57 02-86 08 X 5.23 4.32 3.15 2.26 1.66 1.91	06-18 PCT 94.86 5.83 .66 .19 .85 8.88 00-18 00-18 00-18 1.78 1.74 1.81 .74 .52 .29 .16 .97 .01
X S 1 1 9 9 9 1 5 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	ON 475-3 99-24 99-27 84-63 99-27 84-49 84-49 1 - 33 1 - 35 90-24 1 - 35 90-24	CIUR 10-14 96.98 2.58 2.58 2.58 2.19 2.19 2.19 2.19 2.19 2.19 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10	FEB RI 14-17 99 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PR ATION 22 PG.74 9.259 1.71 9.259 1.73 .78 ATION 2 0.82 1.84 1.88 .83 -81 8.83	22-82 PG-34 12-52 8-35 6-58 2-92 X 7-85 7-97 5-96 4-54 3-52 2-8 1-23 -28 -81	02-66 PCT 78.86 12.68 7.98 5.34 1.59 02-86 08 4.32 3.15 2.36 1.66 .51 .48 .19 .07	06-18 PCT 94.86 5.83 .66 .19 .85 0.00 00 2.19 1.78 1.42 1.81 .74 .52 .29 .16 .07 .02
X 1 9 9 9 7 5 9 9 9 7 5 9 9 9 9 9 9 9 9 9 9	ON ATS-3  9 PC 63 92 4 5 7 5 3 2 6 7 5 3 2 6 7 5 8 6 1 6 7 5 9 2 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	CIUF 10-14 96.98 2.56 96.98 2.56 9.19 9.19 10-14	FE VAR 14-C1 256 05 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PR ATION 16-22 PC.74 9,29 1.71 9,29 1.77 97 2.59 1.78 97 2.59 1.78 4.10 18-2 1.59 2.59 2.59 2.59 2.69 2.69 2.69 2.69	22-82 PCT 64-52 64-55 6-58 2-10 2-0 2 x 7-87 5-54 3-52 2-46 1-23 -85 -82 -82	02-66 PCT 78.86 12.68 7.98 5.34 1.59 02-86 08 4.32 3.15 2.36 1.66 .91 .07	06-18 PCT 94.86 5.83 .66 .19 .05 8.00 8G-18 DB X 2.19 1.74 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.4
X S 1 1 9 9 9 1 5 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	ON 475-3 99-24 99-27 84-63 99-27 84-49 84-49 1 - 33 1 - 35 90-24 1 - 35 90-24	CIUR 10-14 96.98 2.58 2.58 2.58 2.19 2.19 2.19 2.19 2.19 2.19 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10	FEB ARI 14-18 14-18 97.29 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	PR ATION 16-22 PC74 9,29 2.59 1.71 978 4TION 22 08 5.28 4.28 3.35 2.52 1.00 49 .24 .03 -01 8.00 .03	22-82 PCT 64.34 12.52 8.35 6.58 2.41 5.20 22-02 X 7.87 5.95 4.55 2.46 1.23 8.88 1.82 82	02-66 PCT 70.86 12.68 12.68 1.64 1.57 02-86 X 6.34 1.57 02-86 X 6.34 1.66 1.66 1.66 1.67 1.07 1.07	06-18 PCT 94.86 5.83 .66 .19 .85 8.80 00-18 2.19 1.74 1.42 1.81 .74 .52 .29 .16 .07 .02 .01 8.00
X 1999 20-39 20-3	ON ATS -3  9 PC 4 392 47 5	CIUF 10-14 96-98 2-56 9-19 0-19 0-19 10-14	FE VAR 14-C1 256 05 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PR ATION 16-22 PC.74 9,29 1.71 9,29 1.77 97 2.59 1.78 97 2.59 1.78 4.10 18-2 1.59 2.59 2.59 2.59 2.69 2.69 2.69 2.69	22-82 PCT 64-52 64-55 6-58 2-10 2-0 2 x 7-87 5-54 3-52 2-46 1-23 -85 -82 -82	02-66 PCT 78.86 12.68 7.98 5.34 1.59 02-86 08 4.32 3.15 2.36 1.66 .91 .07	06-18 PCT 94.86 5.83 .66 .19 .85 9.80 08 x 2.19 1.78 1.42 1.81 .74 .52 .29 .16 .07 .01 8.00 .01
X S0-399	ON 475 -3 9 PC 6392475 9 PC 6392475 1	CIUR 10-14 96.98 2.56 2.56 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.10 0.19 0.10 0.10	FE VAR 960 P A R I Y 10 1 2 5 6 0 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PR ATION 22 74 72 79 79 79 20 79 20 79 20 79 20 79 20 79 20 79 79 79 79 79 79 79 79 79 79 79 79 79	1969-72 22-01342-52-64-536-5-42-6-5-58-2-6-5-42-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-	02-66 PCT 78.86 12.68 12.68 1.64 1.57 02-86 08 4 5.23 4.32 3.15 2.26 1.66 .51 .48 .19 .07 .07 .03 0.80 81	06-18 PCT 94.86 5.83 .66 .19 .85 8.80 00-18 2.19 1.74 1.42 1.81 .74 .52 .29 .16 .07 .02 .01 8.00
X 50-3-99 T500500000000000000000000000000000000	ON 4 7 3 2 4 3 9 2 4 4 5 5 7 3 2 4 5 5 5 8 7 5 8 7 5 8 7 5 8 9 8 6 7 3 2 3 2 4 5 5 5 8 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	CI UF 10-14 96-98 2-55 9-19 CI UF 10-14 X 10-14 X 10-1	FE VAR R 1 4-T 29 60 60 VAR R 1 97.550 8 0.00 0 VAR R 1 97.550 8 0.00 0 VAR R 1 01.526 1.01 1.01 1.01 1.01 1.01 1.01 1.01 1.0	PR ATION 22 PC.74 9,259 1.713 978 2.591 978 2.592 1.089 4.285 2.584 1.089 -081 9.084 -1.17	1969-72 22-07 22-07 42-55-62-55-62-62-62-62-62-62-62-62-62-62-62-62-62-	2-66 PCT 78.86 12.68 12.68 1.64 1.57 82-86 X 6.34 1.57 82-86 X 6.34 1.57 1.66 1.66 1.97 1.87 1.97 1.97 1.97 1.97 1.97 1.97 1.97 1.9	06-18 PCT 94.86 5.83 .66 .19 .85 8.80 00-18 V2.19 1.74 .52 .29 .16 .07 .02 .01 8.00 .01 .02 .01 8.00
X S9-799 T 500 S0 S	ON 4 732475 X 2 961292120566745552 ON 5 9 961293120566745552 ON 6 9 961245552 ON 6 9 96124552 ON 6 9 96124552 ON 6 9 961245552 ON 6 9 96124550 ON 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	CI UF 10-14 96-98 2-56 96-98 2-56 9-19 0-19 10-14	FE VAR R 14-T 29-60 P VAR R 1 01-561138-125198-128-128-128-128-128-128-128-128-128-12	PR ATION 22 PG 78 2 2 39 2 3 9 2 3 9 2 3 9 3 2 2 3 9 3 2 3 9 3 2 3 2	1969-72 22-013-2-013-2-013-2-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	82-66 PCT 78.86 12.68 12.68 1.64 1.57 82-86 X 8-23 4.32 3.15 2.26 1.66 1.97 1.83 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80	06-18 PCT 94.86 5.83 .66 .19 .85 9.80 08 x 2.19 1.42 1.81 .74 .52 .29 .16 .87 .87 .87 .87 .87 .87 .87 .87
X S0-3999 55000000000000000000000000000000000	ON 4 7.3 2 4 392475 x 2 9612930620500 x 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	CI UF 10-14 96.98 2.56 96.98 2.56 0.19 0.	FE VAR R X 1 4-T 29 6 0 5 0 8 R I X 1 4-T 29 6 0 5 0 8 R I X 1 4-T 20 6 0 8 0 1 2 5	PR AT I ON 22 3 32 5 4 9 4 5 1 1 0 0 8 2 2 5 2 5 2 5 4 5 4 5 1 1 1 1 0 0 5 4 5 2 5 2 5 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1969-72 2 PG 3258 2 PG 3258 3 FG 325	02-66 PCT 78.86 12.68 12.68 13.64 1.57 02-86 08 6.34 4.32 3.15 2.26 1.66 1.97 1.97 1.97 1.98 1.97 1.98 1.97 1.97 1.98 1.97 1.97 1.97 1.97 1.97 1.97 1.97 1.97	06-18 PCT 94.86 5.83 .66 .19 .85 8.88 00 00 2.19 1.78 1.42 1.81 .74 .52 .29 .16 .87 .81 .87 .87 .87 .87 .87 .87 .87 .87 .87 .87
X S9-799 T 500 S0 S	ON 4 732475 X 2 961292120566745552 ON 5 9 961293120566745552 ON 6 9 961245552 ON 6 9 96124552 ON 6 9 96124552 ON 6 9 961245552 ON 6 9 96124550 ON 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	CI UF 10-14 96-98 2-56 96-98 2-56 9-19 0-19 10-14	FE VAR R 14-T 29-60 P VAR R 1 01-561138-125198-128-128-128-128-128-128-128-128-128-12	PR ATION 22 PG 78 2 2 39 2 3 9 2 3 9 2 3 9 3 2 2 3 9 3 2 3 9 3 2 3 2	1969-72 22-013-2-013-2-013-2-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	82-66 PCT 78.86 12.68 12.68 1.64 1.57 82-86 X 8-23 4.32 3.15 2.26 1.66 1.97 1.83 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80	06-18 PCT 94.86 5.83 .66 .19 .85 9.80 08 x 2.19 1.42 1.81 .74 .52 .29 .16 .87 .87 .87 .87 .87 .87 .87 .87

	E-STA NO		UL-YAR	IL	1969-72	rcc1	IL TIME
K=0-3		DIUR	NAL VARIA	TION			
	00-24		14-18 PCY	18-22 PCT	22-02 PC1	92-06 PCT	06-10 PCT
SI 8 <b>8-</b> 19	PCT 90.74		PUI	88.26	81.58	87.86	95.24
	5.34	4.29	96.81 2.90	6.30	7.47	7.09	3.84
40-59	2.01	.61 0	•••	Z.75	4.80	2.86	.69
68-79 88-89	1.01	.03	.03 0.00	1.36 .47	3.18 .96	1.16 .56	.19 .03
90-99	.57	. 33	0.00	. 45	2.10	.44	0.86
		ETUR	NAL VARIA	TION			
	00-24	18-14	14-18	18-22	22-82		
PCT	08 x		DE X		x 68 x		
.05 .10	4.61 3.67	2.14 1.70	1.67 1.36	5.18 4.20	6.38 5.46	4.46 3.61	2.12 1.71
.20	2.73	1.70 1.23 .35 .71 .52 .32 .21 .11 .00 0.00 .00	1.08	3.21 2.06 1.36 .87	4.45	2.78	1.35
	1.71	. 35	•76	2.06	3.69	1.85	•93
1.08	1.14 .71	•71	. 35	1.36	2.15 1.36	1.29	.67 .44
5.00	.33	.32	.19	.40	. 64	. 85 . 42	•32
19.00	.15 A	.21	.10	•17	. 25	.20	. 1 0
28.00	.05 A	-11	.03	. 85	. 03	.07	•03
38.00 48.88	50. Fa	- 32	.18 .03 .02 .04 6.00	.91 03	.25 .03 12 02	• 92 01	.11 .00
50.00	0.00	0.36	0.00	0.08	0.80	8.85	0.68
40	. 04	.02	.02	.04	. 85	.93 .96	.92
78.05	.87	.19	-13	.97	. 97	. 86	•12
88.88 98.88	.87 .09 00 22 73	•12 •04 A	.19 A .28 A .11 A	45	.14 19 E4	.06 .05 07 34	.16 A .14 A
95.00	22	34	.15 A	33	-, 64	34	.01 A
98.90	73	35		93	-1.55	90	31
99.00	-1.28 -1.99	64	42 72	-1.58	-, 64 -1.55 -2.45 -3.63	-1.47	60
99.5¢ 99.8 <b>¢</b>	-1.99 -3.18	-1.44 -1.62	-1.26	-2.37 -3.82	-3.63 -5.68	-2.16 -3.29	-1.02 -1.61
99.98				-5-21	-7.72	-4.36	-2.94
99.95	-4.40 -5.95	-2.10 -2.57	-2.88	-7.02	-9.44	-5.72	-2.55
Kag-3	TON ATS-3		AUG-0	CT	1969-72	FCC	AL TIME
	3	CIU	RNAL VARI	ATICN			
<b>₹≈8</b> ~3		CIU(	RNAL VARI 14-18	ATICN 18-22	22-02	02-06	96-10
K=4-3 SI 80-19	80-24 PCT 86.46	CIU/ 10-14 PCT 91.41	RNAL VARI 14-18 FCT 91.35	ATICN			
SI 80-19 20-39	80-24 PCT 86.46 9.08	CIU/ 10-14 PCT 91.41 7.20	RNAL VARI 14-18 FCT 91.35 7.76	ATICN 18-22 PCT 81.37 11.91	22-02 PC1 78.24 9.91	02-06 PCT 84.67	96-10 PCT 91.39 7.67
SI 81-19 20-39 48-59	80-24 PCT 86.46 9.08 2.23	CIU/ 10-14 PCT 91.41 7.20 .97	RNAL VARI 14-18 FCT 91.35 7.76 .79	ATICN 18-22 PCT 81.37 11.91 3.48	22-02 PCT 78.24 9.91 4.81	02-06 PCT 84.67 19.96 2.80	96-10 PCT 91.39 7.67
SI 81-19 20-39 40-59 68-79	80-24 PCT 86.46 9.08	CIU/ 10-14 PCT 91.41 7.20	RNAL VARI 14-18 FCT 91.35 7.76	ATICN 18-22 PCT 81.37 11.91	22-02 PC1 78.24 9.91	02-06 PCT 84.67	96-10 PCT 91.39 7.67
SI 80-19 20-39 48-59 68-79	90-24 PCT 96.46 9.08 2.23	CIUI 10-14 PCT 91.41 7.20 .97	RNAL VARI 14-18 FCT 91.35 7.76 .79	ATICN 18-22 PCT 81.37 11.91 3.48 1.34	22-92 PCT 78.24 9.91 4.81 3.48	02-06 PCT 84.67 18.96 2.80	96-10 PCT 91.39 7.67 .66
SI 81-19 20-39 40-59 68-79	90-24 PCT 86.46 9.08 2.23 1.17 .41	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35	RNAL VARI 14-18 PCT 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43	02-06 PCT 84-67 18-06 2-80 1-74 -19	96-10 PCT 91.39 7.67 .66 .23
SI 80-19 20-39 48-59 68-79 48-89 99-99	80-24 PCT 86-46 9-08 2-23 1-17 -41 -64	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35 .45	RNAL VARI 14-18 FCT 91.35 7.76 .79 .89 0.00 0.00 RNAL VARI 14-18	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43	02-06 PCT 84.67 18.06 2.20 1.74 .19 .53	06-10 PCT 91.39 7.67 .66 .23 .05 V.30
SI 81-19 20-39 40-59 68-79	90-24 PCT 86.46 9.08 2.23 1.17 .41	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35 .35	RNAL VARI 14-18 PCT 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43	02-06 PCT 84.67 10.06 2.20 1.74 .19 .53	06-10 PCT 91.39 7.67 .66 .23 .05 U.30
K=U+3 SI 19 20-39 48-59 68-79 88-89 98-99	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 08 x 4.79 3.86	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35 .35 .15	RNAL VARI 14-18 FCT 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI 14-18 CC X 2.18	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 93 ATION 18-22 CB 5.44 4.42	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X CB X 5.71	02-06 PCT 84-67 19-06 2-20 1-74 -19 -53 08 X 4-53 3-68	96-10 PCT 91.39 7.67 .66 .23 .05 V.20 96-18 DB X 2.34
K=U+3 SI 19 20-39 40-59 68-79 80-89 PCT - 45 - 29	80-24 PCT 86-46 9.08 2.23 1.17 .41 .64	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35 .35 .35 .35	RNAL VARI 14-18 PCT 91.35 .79 .89 8.08 0.30 RNAL VARI 14-18 CC X 2.18 1.83 1.51	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 CB 5.44 4.42 3.49	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X CB X 5.87 5.71	02-06 PCT 84.67 19.06 2.20 1.74 .19 .53 82-86 08 x 4.53 3.68 2.82	96-10 PCT 91.39 7.67 .66 .23 .95 V.30 96-18 DB x 2.34 1.91 1.54
K=U+3 SI 19 20-39 40-59 68-89 99-99 PCT 5-189 -29	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 08 x 4.79 3.86 2.92 1.88	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35 .05 DIUI 18-14 C.36 2.37 i.64	RNAL VARI 14-18 FCT 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI 14-18 CE X 2.18 1.83 1.51 1.12	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 CB 5.44 4.42 3.49 2.33	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X 6.86 5.71 4.65 3.32	02-06 PCT 84.67 18.86 2.20 1.74 .19 .53 02-86 08 x 4.53 3.68 2.82 1.98	06-10 PCT 91.39 7.67 .66 .23 .05 U.20 86-18 DB x 2.34 1.91 1.54
K=U+3 SI 19 20-39 48-59 68-79 88-89 PCT - 05 - 18 - 29 - 18 - 29 - 18 - 29 - 29 - 29 - 29 - 29	80-24 PCT 86-46 9.08 2.23 1.17 .41 .64	CIUI 10-14 PCT 91.41 7.20 .97 .32 .35 .35 .35 .35	RNAL VARI 14-18 PCT 91.35 .79 .89 8.08 0.30 RNAL VARI 14-18 CC X 2.18 1.83 1.51	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 CB 5.44 4.42 3.49	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X CB X 5.87 5.71	02-06 PCT 84.67 19.06 2.20 1.74 .19 .53 82-86 08 x 4.53 3.68 2.82	96-10 PCT 91.39 7.67 .66 .23 .95 V.30 96-18 DB x 2.34 1.91 1.54
K=1+3 SI-39 -39 -8-59 -8-79 -88-89 F -38 -38 -38 -38 -38 -38 -38 -38 -38 -38	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 08 x 4.79 3.86 2.92 1.88 1.30 .49	0-14 PCT 91.41 7.20 .97 .32 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35	RNAL VARI 14-18 FCT 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI 14-18 CC 2.18 1.63 1.51 1.64 .38	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 ATION 18-22 S.44 4.42 3.49 2.33 1.62 1.65	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X CB 86 5.71 4.65 3.35 1.52	02-06 PCT 84-67 18-06 2-80 1-74 -19 -53 82-86 08 X 4-53 3-68 2-82 1-90 1-36 -94 -53	96-10 PCT 91.39 7.67 .66 .23 .05 V.30 86-18 DB x 2.34 1.91 1.54 1.13 .86 .64
X=1+3 SI-39 20-39 48-79 68-89 90-99 PCT-35 -50 1.50 2.00 10.00	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 x 4.79 3.86 2.92 1.88 1.30 .89 .29 A	CIUI 10-14 PCT 91.41 7.20 .97 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35	RNAL VARI 14-18 FCT 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI 14-18 CE X 2.18 1.83 1.51 1.12 .64 .38 .23	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 CB 5.44 4.42 3.49 2.33 1.62 1.62 5.64	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X 6.86 5.71 4.65 3.32 2.35 2.35 2.35 2.32	02-06 PCT 84.67 18.06 2.20 1.74 .19 .53 82-86 08 x 4.53 3.68 2.82 1.90 1.36 .94	06-10 PCT 91.39 7.67 .66 .23 .05 V.30 06-18 DB x 2.34 1.91 1.54 1.13 .46 .64 .39
K=1+3 SI-39 -39 -8-59 -8-79 -88-89 F -38 -38 -38 -38 -38 -38 -38 -38 -38 -38	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 08 x 4.79 3.86 2.92 1.88 1.30 .49	0-14 PCT 91.41 7.20 .97 .32 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35	RNAL VARI 14-18 FCT 91.35 7.76 .79 8.08 0.00 RNAL VARI 14-18 2.18 1.61 1.51 1.51 1.51 1.51 1.51	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 CB 5.44 4.42 3.43 1.62 1.65 .61	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X 6.86 5.71 4.65 3.35 1.52 2.35 1.52 3.35 1.52	02-06 PCT 84.67 18.96 2.20 1.74 .19 .53 82-86 08 4.53 3.68 2.82 1.98 1.36 .53 .38	06-10 PCT 91.39 7.67 .23 .25 V.20 86-18 DB X 2.34 1.91 1.54 1.13 .86 .64 .39
K=1+3 9-39 9-39 9-39 9-79 9-89 1-38 9-1-38 10-88 10-88 10-88 10-88 10-88	80-24 PCT 86-46 9.08 2.23 1.17 .64 .64 .65 .80 2.92 1.80 .49 .49 .49 .49 .49 .49 .49 .49 .49	CIUI 10-14 PCT 91.41 7.20 .97 .35 .35 .35 .35 .35 .37 .46 10-14 .96 .96 .98 .98 .98 .98 .99	RNAL VARI 14-18 91.35 7.76 .79 .89 8.08 0.30 RNAL VARI 14-18 2.18 1.83 1.51 1.12 .56 .64 .38 .23	ATICN 18-22 PGT 81:37 11:91 3-48 1.34 -97 ATION 10-22 CB 5:44 4:42 3:49 2:33 1:62 1:69 -36 -36	22-02 PCT 78-24 9.91 4.81 3.48 1.21 2.43 22-02 x CB 6.86 5.71 4.65 3.32 2.35 1.52 .82 .83 .84	02-06 PCT 84.67 19.06 2.80 1.74 .19 .53 82-86 X 4.53 3.68 2.82 1.90 1.36 .94 .53 .38	06-10 PCT 91.39 7.67 .66 .23 .05 V.30 06-18 DB x 2.34 1.91 1.54 1.13 .46 .64 .39
X = 1 + 3 SI - 3 9 20 - 3 9 20 - 3 9 80 - 9 9 90 - 9 7 50 - 10 9 10 9 10 - 10 9 10	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 x 4.78 2.92 1.80 1.30 .49 .49 .49 .49 .49 .49 .49 .49 .49 .49	CIUI 10-14 91.41 9	RNAL VARI 14-18 91-35 7-76 -79 -89 -0-30 RNAL VARI 14-18 2-18 1-12 -64 -38 -23 -11 -64 -38 -38 -38	ATICN 18-22 PGT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 5.44 4.42 3.49 2.33 1.62 1.62 68 688	22-02 PCT 78.24 9.91 3.48 1.21 2.43 2.88 5.71 4.65 3.32 2.35 2.35 2.35 2.35 2.35 2.35 2.3	02-06 PCT 84.67 18.06 2.20 1.74 .19 .53 08-86 08 x 4.53 3.68 2.82 1.90 1.36 .94 .53 .82	06-10 PCT 91.39 7.67 .66 .23 .05 V.30 06-18 DB x 2.34 1.91 1.54 1.13 .86 .64 .39 .24 .12 .85
T 199	80-24 PCT 86-46 9.08 2.23 1.17 .64 .64 .65 .87 3.86 2.92 1.80 .49 .49 .49 .49 .49 .49 .49	CIUI 10-14 PCT 91.41 7.20 .97 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35	RNAL VARI 14-18 91.35 7.76 .79 8.08 0.30 RNAL VARI 14-18 2.18 1.51 1.51 1.51 1.51 1.64 .38 .38 .38 .38 .38	ATICN 18-22 PCT 81.37 11.91 3.48 1.34 1.37 .97 .93 ATION 18-22 5.44 4.42 3.33 1.62 1.62 1.62 1.63 .88 .88	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 X 6.86 5.71 4.65 3.32 2.35 1.52 2.35 1.52 2.01 0.01	02-06 PCT 84.67 18.86 2.20 1.74 .19 .53 08-86 08 4.53 3.68 2.82 1.90 1.36 .94 .53 .30 .14 .67	06-10 PCT 91.39 7.67 .23 .25 U.20 86-18 DB X 2.34 1.91 1.54 1.13 .86 .64 .39 .24 .12 .85
X = 1 + 3 SI - 3 9 20 - 3 9 20 - 3 9 80 - 9 9 90 - 9 7 50 - 10 9 10 9 10 - 10 9 10	80-24 PCT 86.46 9.08 2.23 1.17 .41 .64 80-24 x 4.79 3.86 2.92 1.88 1.30 .49 .49 .49 .49 .49 .49 .49 .49 .49 .49	CIUI 10-14 91.41 9	RNAL -18	ATICN 18-22 PGT 81.37 11.91 3.48 1.34 .97 .93 ATION 18-22 5.44 4.42 3.49 2.33 1.62 1.62 68 688	22-02 PCT 78.24 9.91 3.48 1.21 2.43 2.88 5.71 4.65 3.32 2.35 2.35 2.35 2.35 2.35 2.35 2.3	02-06 PCT 84.67 18.06 2.20 1.74 .19 .53 08-86 08 x 4.53 3.68 2.82 1.90 1.36 .94 .53 .82	06-10 PCT 91.39 7.67 .23 .25 U.20 86-18 DB X 2.34 1.91 1.54 1.13 .86 .64 .39 .24 .12 .85
T 999 99 5 100 100 100 100 100 100 100 100 100 1	80-24 PCT 86.46 9.08 2.23 1.17 .64 .65 80-24 x 08 4.79 3.86 2.92 1.88 1.30 .49 .49 .29 A .29 A	CIUI 10-14 91.41 9	RNAL 14-18 91-769-89 0.00 VAR 14-18 X 14-18 X	ATION 18-22 PCT 81.37 11.91 3.48 1.34 .97 .93 ATION 22 CB 5.44 2.33 1.62 2.33 1.62 .16 .88 .8188	22-02 PCT 78.24 9.91 3.48 3.48 2.43 2.88 5.71 4.65 2.87 3.32 2.35 2.35 2.35 2.35 2.35 2.35 2.35	02-06 PCT 84.67 19.06 2.20 1.74 .19 .53 08-86 X 3.68 2.82 1.98 1.36 .98 .98 .98 .98	06-10 PCT 91.39 7.67 .23 .25 U.20 86-18 DB X 2.34 1.91 1.54 1.13 .86 .64 .39 .24 .12 .85
T 1999 5588 510.88 89 89 80 80 80 80 80 80 80 80 80 80 80 80 80	80-24 PCT 86.46 9.08 2.23 1.17 .64 80-24 x 3.86 2.92 1.88 1.30 .49 .49 .49 .49 .49 .49 .49 .49 .49 .49	CIUI 10-14 91.41 92.42 93.35 93.35 93.35 94.41 18-14 18-14 18-14 96.65 96 96.65 96 96 96 96 96 96 96 96 96 96 96 96 96	RNAL 14-18 97-769 8.08 8.09 8.00 8.14-18 91-18-18-18-18-18-18-18-18-18-18-18-18-18	ATION 18-22 PCT 11.91 3.48 1.347 .993 ATION 22 5.44 5.49 2.33 1.62 1.62 1.68 .88 .88 .88 .88 .88 .88 .88 .88 .88	22-G2 PCT 78.24 9.91 4.81 3.43 2-02 X 5.68 5.75 4.65 2.35 2.35 2.35 2.35 2.35 2.35 2.35 2.3	02-06 PCT 84.67 18.86 2.20 1.74 .19 .53 3.68 2.82 1.90 1.36 .91 .82 .82 .82 .80 .80 .80 .80 .80 .80 .80 .80 .80 .80	06-10 PCT 91.39 7.67 .23 .25 U.90 86-18 DB X 2.34 1.91 1.54 1.13 .86 .64 .39 .24 .12 .85 .85 .86 .86 .86 .86 .86
T 999 99 5 100 100 100 100 100 100 100 100 100 1	80-24 PCT 86.46 9.08 2.23 1.17 .64 .65 80-24 x 08 4.79 3.86 2.92 1.88 1.30 .49 .49 .29 A .29 A	CIUI 10-14 91.41 9	RNAL 14-18 91-769-89 0.00 VAR 14-18 X 14-18 X	ATICN 18-22 PCT 11.91 3.48 1.34 1.37 .93 ATION 18-22 5.44 4.42 3.43 1.62 1.62 1.62 1.63 .08 0.818387 -1.23	22-02 PCT 78.24 9.91 4.81 3.48 1.21 2.43 22-02 x 5.71 4.65 2.35 2.35 2.35 2.35 2.35 2.35 2.35 2.3	02-06 PCT 84.67 18.86 2.80 1.74 .19 .53 82-86 X 3.68 2.82 1.98 1.36 .87 .87 .88 .87 .88 .87	06-10 PCT 91.39 7.67 .23 .25 U.20 86-18 DB 2.34 1.91 1.54 1.54 1.54 1.54 1.54 1.54 1.54 1.5
T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	80-24 PCT 86.46 9.08 2.23 1.17 .64 .65 .65 .65 .65 .65 .65 .65 .65 .65 .65	10-14 91.41	RNAL 4-18 97.769 - 89 - 0.00 - 18 - 1	ATION 18-22	2-02 78.24 9.91 3.48 3.48 2.88 5.75 2.88 5.75 3.32 2.88 5.75 3.32 48 -01 0.88 -02 -1.72 -1.28 -1.28 -1.29	02-06 PCT 84.67 18.06 2.20 1.74 .53 08-86 X 53.58 2.82 1.90 1.36 .53 .53 .14 .07 .08 .08 .08 .09 .09 .00 .00 .00 .00 .00 .00 .00 .00	06-10 PCT 91.39 7.67 .23 .25 U.90 86-18 DB X 2.34 1.91 1.54 1.13 .86 .64 .39 .24 .12 .85 .85 .86 .86 .86 .86 .86
T - 3 - 3 - 3 - 3 - 3 - 3 - 3 - 3 - 3 -	80-24 PCT 86.46 9.08 2.23 1.17 .64 80-24 x 80-24 x 80-24 x 1.30 80-24 x 1.30 80 80 80 80 80 80 80 80 80 80 80 80 80	10-17 91.41 92.41 92.41 93.45 93.35 94.41 18-14	RNAL 14-18 97.769 8.00 8.00 8.00 8.00 8.00 8.00 8.00 8.0	ATION 22 PCT 11.91 3.48 1.347 .93 22 4.49 2.33 1.62 2.33	2-02 78.24 9.91 3.48 3.43 2-02 6.01 3.32 2.86 5.75 3.32 3.35 4.65	02-06 PCT 84.67 18.86 2.20 1.74 .53 08-86 X 3.68 2.82 1.90 1.36 .53 .30 .14 .82 46 18 46 18 18 18 18 18 18 18 18	06-10 PCT 91.39 7.67 .23 .25 U.20 86-18 DB 2.34 1.91 1.13 .86 .64 .39 .24 .12 .85 .85 .86 .86 .86 .86 .86 .86 .86 .86 .86 .86
T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	80-24 PCT 86.46 9.08 2.23 1.17 .64 .65 .65 .65 .65 .65 .65 .65 .65 .65 .65	10-14 91.41	RNAL 4-18 97.769 - 89 - 0.00 - 18 - 1	ATION 18-22	2-02 78.24 9.91 3.48 3.48 2.88 5.75 2.88 5.75 3.32 2.88 5.75 3.32 48 -01 0.88 -02 -1.72 -1.28 -1.28 -1.29	02-06 PCT 84.67 18.06 2.20 1.74 .53 08-86 X 53.58 2.82 1.90 1.36 .53 .53 .14 .07 .08 .08 .08 .09 .09 .00 .00 .00 .00 .00 .00 .00 .00	06-10 PCT 91.39 7.67 .623 .05 U.30 06-18 DB X 2.34 1.91 1.94 1.13 .86 .64 .39 .24 .12 .85 .80 .80 .80 .80 .80 .80 .80 .80 .80 .80

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HAMILTON ATS-	.3	ALL D	ATA	1969-72	LCGA	L TIME
K=0-3	DIU	MAL VARI	ATION			
10-24	10-14	14-18	18-22	25-05	02-06	06-10
SI PCT 00-19 86.61	PÇT 94.57	PCT 94.24	PCT 85.66	PCT 72.65	PCT 79.49	PCT 92.92
20-39 8.00	4.40	5.26	8.90	11.76	11.70	5.95
43-59 2.77 60-79 1.43	.70 .15	.43 .06	2.76 1.33	7.05 4.31	4.77 2.55	.90 .19
80-89 .45	16	.01	.63	1.30	.69	.03
99-99 .74	• • 3	3.00	.72	2,93	.80	.01
	GIU	RNAL VARI				
09-24	19-14	14-18	1122		02-06 DB X	06-10
PCT DB	X DB X	DB X	08 ) 5.01	7.11	5.22	DB X 2.29
.10 4.05	1.78	1.62	4.87	6.88	4.31	1.68
.20 7.10 .50 2.92	1.40 .98	1.32 .96	3.13 2. <b>8</b> 5	4.91 3.61	3.43 2.38	1.50 1.08
1.00 1.39	.76	.73	1.42	2.61	1.72	.81
2.00 .91	.51	.53	.94	1.75	1.18	-58
5.00 .46 18.80 .24	.29 .17	•31 •18	.49 .26	.90 .45	.65 .35	.33 .19
29.06 .10	. i S	.08	.11	.15	-15	.18
39.00 .05 40.0001	.34 .86	.04 .01	.85 81	.05 .01	.07 .01	.03 .01
40.0001 50.90 0.00	0.96	0.00	0.00	8.80	0.00	9.09
62.00 .93	. 32	.01	.03	. 61	. 80	.01
70.00 .04	.39	.09	.03	01 10	. 81 05	.88 .99 A
98.8012	. P . A			43	28	.03 Ä
95.0040	05	07 A		97	64	14 A
98.0098 99.00 -1.60	36 67	39 66	-1.82 -1.64	-2.99 -2.99	-1.34 -2.00	49 82
99.56 -2.33	-1.39	-1.05	-2.30	-4.31	-2.76	-1.25
99.80 -3.67	-1.69	-1.61	-3.74	-6.53	-4.10	-1.63
99.90 -4.95	-2.18 -2.68	-2.02 -2.41	-5.83 -6.71	-8.45 -18.44	-5.34 -7.84	-2.30 -2.76
HAMILTON AT: K=4,9	5-3	ALL	DATA	1969-72	LOC	CAL TIME
K=4,9	CI	URNAL VAT	TATION			
	CI( 18-14	URNAL VAT	NOITAI'	22-02	02-06	06-10
K=4,9 BC-24 SI PCT BC-19 75.21	CI( • 18-14 PST • 93.J1	URNAL VAT 14-18 PCT 89.26	TATION 18-22 FCT 79.05	22-02 PCT 60.54	02-06 PCT 53.15	06-10 PCT 78.12
K=4,9 00-2- SI PCT 00-19 75-2- 20-39 13-5-	CI( 18-14 PST 8 93.J1 5 5.72	URNAL VAT 14-18 PCT 89.26 7.72	TATION 18-22 FCT 79-05 10-79	22-02 PCT 60.54 19.13	02-06 PCT 53.15 21.59	06-10 PCT 78.12 17.23
K=4,9 BC-24 SI PCT BC-19 75.21	CIO 10-14 PCT 93.72 9.72 9.1.13 9.24	URNAL VAT 14-18 PCT 89.26 7.72 2.25	TATION 18-22 FCT 79.05	22-02 PCT 60.54	02-06 PCT 53.15	06-10 PCT 78.12
K=4,9 80-2 SI PCT 00-19 75.2 20-39 13.55 40-59 5.0 68-79 2.6 88-89 1.1	CII 18-14 PCT 93.J1 5.72 9 1.J3 6 .24 8 0.J0	URNAL VAT 14-18 PCT 89.26 7.72 2.25 .63 .07	PIATION 18-22 FCT 79.05 10.79 4.29 2.46	22-02 PCT 60.54 19.13 7.16 4.75 2.91	92-96 PCT 53.15 21.59 12.59 6.86 2.15	06-10 PCT 78.12 17.23 2.07 1.29
K=4,9 80-2 SI PCT 00-19 75.2 20-39 15.0 40-59 5.0 60-79 2.6	CII 18-14 PCT 93.J1 5.72 9 1.J3 6 .24 8 0.J0	URNAL VAT 14-18 PCT 89.26 7.72 2.25	PIATION 18-22 FCT 79.05 10.79 4.29 2.46	22-02 PCT 60.54 19.13 7.16 4.75	02-06 PCT 53.15 21.59 12.59 6.06	06-10 PCT 78.12 17.23 2.87 1.29
K=4,9  8C-C SI PCT 00-19 75.2 20-39 13.5 40-59 5.0 60-79 2.6 80-89 1.1 90-99 2.2	CI( 18-14 PCT 8 93.J1 5 5.72 9 1.J3 6 24 8 0.J0 0.10	URNAL VA" 14-18 PCT 89-26 7-72 2-25 -63 -07 -87	PATION 18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46	22-02 PCT 60.54 19.13 7.16 4.75 2.91	02-06 PCT 53-15 21-59 12-59 6-86 2-15 4-46	06-10 PCT 78.12 17.23 2.07 1.29 .30
K=4,9 80-2 SI PCT 00-19 75.2 20-39 13.55 40-59 5.0 68-79 2.6 88-89 1.1	CI(  18-14  PCT  93.J1  5.72  1.J3  6.J0  0.00  CI(  10-14	URNAL VA <sup>1</sup> 14-18 PCT 89.26 7.72 2.25 .07 .63 .07 .67 URNAL VAR 14-18	18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46	22-02 PCT 60.54 19.13 7.16 4.75 2.51 5.51	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.44	05-10 PCT 78.12 17.23 2.07 1.29 .30 .20
SI PCT 00-19 75.2: 20-39 13.5: 40-59 5.0: 60-79 2.6: 80-89 1.1: 90-99 2.2:	CI(  18-14  PCT  93.J1  5.72  1.J3  .24  9.30  CI(  10-14  x OB  2.27	URNAL VA" 14-18 PCT 69.26 7.72 2.25 .63 .07 .87  JRNAL VAR 14-18 K CB 3.88	18-22 FCT 79-05 10-79 4-29 2-46 2-46 2-46 IATION 18-22 X CB 6-82	22-02 PCT 60.54 19.13 7.16 4.75 2.51 5.51 22-02 X 08 7.81	02-06 PCT 53-15 21-59 12-59 6-86 2-15 4-46	05-10 PGT 78.12 17.23 2.07 1.29 .30 .20
SI PCT 00-19 75.2: 20-39 13.5; 40-59 5.0: 60-79 2.6: 80-89 1.1: 90-99 2.2: PCT 08 .05 6.7; .10 5.6:	CI( PCT	URNAL VA" 14-18 4-17 69.26 7.72 2.25 .63 .07 .07 JRNAL VAR 14-18 4 CB 3.88 2.46	18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATICN 18-22 X CB 6.42 5.68	22-02 PCT 60.54 19.13 7.16 4.75 2.51 5.51 22-02 X 08 7.41 7.01	92-06 PCT 53.15 21.59 12.59 6.86 2.15 4.44 92-06 X OB 7	06-10 PCT 78.12 17.23 2.07 1.29 .30 .20
SI PCT 00-19 75.2: 20-39 13.5: 40-59 5.0: 60-79 2.6: 80-89 1.1: 90-99 2.2:	CI(  18-14 PCT 93.J1 5.72 1.J3 6.J0 0.30 CI( 10-14 X OB 2.27 1.68 1.52	URNAL VA" 14-18 PCT 69.26 7.72 2.25 .63 .07 .87  JRNAL VAR 14-18 K CB 3.88	18-22 FCT 79-05 10-79 4-29 2-46 2-46 2-46 IATION 18-22 X CB 6-82	22-02 PCT 60.54 19.13 7.16 4.75 2.51 5.51 22-02 X 08 7.81	02-06 PCT 53.15 21.59 12.59 6.06 2.15 4.44	06-10 PCT 78.12 17.23 2.07 1.29 .30 .20
SI PCT 00-19 75.2 20-39 13.5 40-59 5.0 60-79 2.6 80-89 1.1 90-99 2.2 PCT 08 .05 6.7 .10 5.6 .20 4.5 .50 3.2 1.00 2.2	CI(  18-14 PCT 93.J1 5.72 1.J3 6.3 9.J0 9.J0 18-14 X 08 2.27 1.88 1.52 1.39 6.01	URNAL VA <sup>*</sup> 14-18 PGT 69.26 7.72 2.25 .63 .67 .87 URNAL VAR 14-18 K CB 3.88 2.46 1.96	1ATION 18-22 FCT 79.05 10.79 4.29 2.46 2.46 IATION 18-22 X CB 6.62 5.68 4.61 3.23 2.22	22-02 PCT 60.54 15.13 7.16 4.75 2.51 22-02 X 200 7.81 7.81 5.90 3.43	02-06 PCT 53.15 21.59 12.59 6.06 2.15 4.45 82-06 X OB ) 7.62 6.69 5.57 4.22 3.20	06-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 x 3.81 3.13 2.51 1.68 1.37
SI PCT 00-19 75.2: 20-39 13.5; 40-59 5.0: 60-79 2.6: 80-89 1.1: 90-99 2.2: PCT 08 .05 6.7; .10 5.6: .20 4.5; .50 3.2: 1.00 2.2:	CI(  18-14  PCT  93.J1  5.72  1.J3  .24  9.30  CI(  10-14  X 08  2.27  1.88  1.32  1.32  1.32	URNAL VA <sup>*</sup> 14-18 PCT 69.26 7.72 2.25 .63 .07 .87  JRNAL VAR 14-18 K CB 3.28 2.46 1.96 1.40 1.04 .73	IATION 18-22 FCT 79.05 10.79 4.29 2.46 2.46 2.46 3.45 3.23 3.23 2.42	22-02 PCT 60.54 19.13 7.16 4.75 2.51 22-02 X 08 7.81 5.98 4.58 3.43 2.39	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.46 02-06 X 08 7.62 6.69 5.57 4.22 3.20 2.20	06-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 0.00 x 3.81 3.13 2.51 2.60 1.37
K=4,9  SI PCT 00-19 75.2 20-39 13.5 40-79 2.6 88-89 1.1 93-99 2.2  PCT D8 .05 6.7 .10 5.6 .20 4.5 .50 3.2 1.00 2.2 2.00 1.4 5.00 .41	CI(  18-14  93. J1  5. 72  1. J3  6. J0  9. 30  10-14  X 08  2. 27  1. 52  1. 39  1. 31  1. 52  1. 39  1. 31  1. 52	URNAL VAP 14-16 PCT 69.26 7.72 2.25 .63 .07 .87  URNAL VAR 14-18 X CB 3.88 2.46 1.49 1.94 .73 .41	IATION 18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATION 18-22 X CB 6.42 5.68 4.61 3.23 2.22 1.42 .32	22-02 PCT 60.54 19.13 7.15 2.91 5.51 22-02 X 7.81 7.81 5.90 4.50 3.43 2.39 1.65	02-06 PCT 53.15 21.59 12.59 6.06 2.15 4.45 82-06 X OB ) 7.62 6.69 5.57 4.22 3.20	06-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 x 3.81 3.13 2.51 1.68 1.37
K=4,9  SI PCT 00-19 75.2 20-39 13.5 40-59 5.6 88-89 1.6 98-99 2.2  PCT D8 .85 6.7 .10 5.6 .20 2.2  1.88 2.2 2.80 1.4 20.09 .1	CI(  18-14  93.J1  5.72  1.J3  .24  3.0.J0  0.J0  18-14  x.08  2.27  1.88  1.52  1.39  .01  .56  .36  .36	URNAL VA <sup>*</sup> 14-18 PCT 69.26 7.72 2.25 .63 .67  JRNAL VAR 14-18 1.08 2.46 1.96 1.94 1.04 .73 .41	IATION  18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATION 18-22 X CB 6.62 5.68 4.61 3.23 2.22 1.42 .68 .31	2 - 02 - 00 - 54 15 - 13 7 - 15 2 - 02 7 - 01 7 - 01 7 - 01 7 - 01 7 - 01 7 - 01 1 - 01 1 - 01 2 - 02 2 - 03 2	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 82-06 X OB 7.62 6.69 5.57 4.22 3.28 2.20 1.39	06-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 3.81 3.13 2.51 1.37 1.02 .65 .42
R=4,9  SI PCT 00-19 75.2 20-39 13.5 40-59 2.6 60-79 2.6 60-89 1.1 90-99 2.2  PCT D8 .50 5.6 .20 4.5 .2	CI(  18-14 PCT 93.J1 5.72 1.J3 6.J0 0.J0 CI( 18-14 X OB 2.27 1.48 1.52 1.39 1.39 1.39 1.36 1.36 1.36 1.36 1.36 1.36 1.36 1.36	URNAL VAP 14-16 PGT 69.26 7.72 2.25 .63 .07 .87  URNAL VAR 14-18 X CB 3.88 2.46 1.49 1.94 .73 .41	IATION 18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATION 18-22 X CB 6.42 5.68 4.61 3.23 2.22 1.42 .32	22-02 PCT 60.54 19.13 7.15 2.91 5.51 22-02 X 7.81 7.81 5.90 4.50 3.43 2.39 1.65	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.46 82-06 X OB 7.62 6.69 5.57 4.22 3.28 2.28 1.39	05-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 x 3.81 3.13 2.51 2.65 1.37 1.02 .65
K=4,9  80-2  SI PCT 00-19 75.2 20-39 13.5 40-29 2.6 80-89 1.1 93-99 2.2  PCT D8 .05 6.76 .20 4.5 .50 3.2 1.00 2.2 2.00 1.41 5.00 .11 20.09 .11 20.09 .15	CI(  18-14  93. J1  5. 72  1. J3  6. J0  9. 30  10-14  X	URNAL VAP 14-16 PCT 69.26 7.72 2.25 .63 .07 .67  URNAL VAR 14-18 X CB 3.88 2.46 1.49 1.04 .73 .41 .27 .89	IATION  18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATION 18-22 X CB 6.62 5.66 4.61 3.23 2.22 1.42 .03 -03 -03 8.00	2 - 0 2	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.46 82-06 X DB 7.62 6.69 5.57 4.22 3.28 1.39 .75 .36	05-10 PGT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 X 3.81 3.13 2.51 1.08 1.37 1.08 .22 .22
K=4,9  SI PCT 00-19 75.2 20-39 13.5 40-59 5.6 88-89 1.1 98-99 2.2  PCT D8 .05 6.7 .10 5.6 .20 4.6 .50 3.2 1.00 2.2 2.00 1.4 2.00 1.4 2.00 .7 18.00 .6 20.09 .1 30.00 .0 50.00 .0	CI(  18-14  93. J1  5.72  1. J3  6. 24  9. J0  18-14  X 08 7  1. 80  1. 52  1. 139  1. 81  1. 72  1. 16  1. 52  1. 139  1. 16  1. 52  1. 139  1. 16  1. 30  1. 31	URNAL VA <sup>*</sup> 14-18 69.26 7.72 2.25 .63 .67 .87  URNAL VAR 14-18 X 3.88 2.46 1.48 1.96 1.49 1.04 .73 .41 .87 .89 .84	IATION  18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATION 18-22 X 68.42 5.68 4.61 3.23 2.22 1.42 .68 9.03	2 - 0 2	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 82-06 X 7.62 6.69 5.57 4.22 3.20 2.28 2.28 2.39	05-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 x 3.81 3.13 2.51 2.60 1.37 1.02 .65 .42 .22 .03 6-10
K=4,9  SI PCT 00-19 75.2: 20-39 13.5: 40-59 5.6: 60-79 2.6: 80-89 1.2: 90-99 2.2:  PCT 08-2: PCT 08-2: 1.00 2.2: 1.0	CI(  18-14  93.J1  5.72  1.J3  6.J0  9.30  CI(  18-14  2.27  1.48  1.52  1.39  .31  0.93  .31  0.93  .31  0.93  .31	URNAL VA <sup>*</sup> 14-18 9000 14-18 1	IATION  18-22 FCT  79.05 10.79 4.29 2.46 2.46 2.46 3.08 6.82 5.66 4.61 3.22 1.42 .64 .32 .93 -82 8.08	2 PC T 4 15 13 PC T 6 PC T 6 PC T 6 PC T 7 15	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 02-06 3.7.66 9.57 4.22 3.28 2.28 1.39 -75 .36 .96 8.88 85 14	05-10 PGT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 X 3.81 3.13 2.51 1.08 1.37 1.08 .22 .22
R=4,9  SI PCT 00-19 75.2 20-39 13.5 40-29 2.6 80-89 1.1 93-99 2.2  PCT D8 .05 6.76 .10 5.7 .10 2.2 .10 2.2 .10 2.2 .10 2.2 .10 3.2 .10	CI(  18-14  93.J1  5.72  1.J3  6.J0  9.30  CI(  10-14  X OB 7  1.39  1.39  1.39  1.39  1.39  1.30  1.30  1.30  1.30  1.30  1.30  1.30  1.30  1.30  1.30  1.30	URNAL VAP 14-16 89.26 7.72 2.25 .63 .63 .67 .87  URNAL VAR 14-18 X CB 3.88 2.46 1.48 1.04 .73 .41 .27 .89 .81 8.08 .81	IATION  18-22 FCT 79.05 10.79 4.29 2.46 .95 2.46 IATION 18-22 X CB 6.62 5.66 4.61 3.23 2.22 1.42 .03 .03 .03 .03 .03 .03 .03 .03 .03 .03	2 PCT 437 7 175 4 175 1 2 2 8 4 1 1 2 2 8 3 4 3 9 5 4 5 8 3 4 3 9 5 4 6 5 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 82-06 X DB 7.62 5.57 4.22 3.28 2.28 1.39 .75 .36 .18 .18 .18 .18 .18 .18 .18 .18 .18 .18	05-10 PGT 78.12 17.23 2.07 1.29 .20 86-10 86-10 X 3.81 3.51 1.02 .65 .42 .22 .84 .03 .00 .00 .00 .00 .00 .00 .00 .00 .00
K=4,9  SI PCT 00-19 75.2: 20-39 13.5: 40-59 5.6: 60-79 2.6: 80-89 1.2: 90-99 2.2:  PCT 08-2: PCT 08-2: 1.00 2.2: 1.0	CI(  18-14  93. J1  5. 72  1. J3  6. J0  9. J0  18-14  X 08 7  1. 52  1. 152	URNAL VAP 14-16 89.26 7.72 2.25 .63 .63 .67 .87  URNAL VAR 14-18 X CB 3.88 2.46 1.48 1.04 .73 .41 .27 .89 .81 8.08 .81	IATION  18-22 FCT  79.05 10.79 4.29 2.46 2.46 2.46 3.08 6.82 5.66 4.61 3.22 1.42 .64 .32 .93 -82 8.08	2 PCT 433 2 PCT 433 7 • 155 15 • 155 2 PB 411 2 PB 433 3 • 4325 4 • 4	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 82-06 X 7.62 6.69 5.57 4.22 3.28 2.28 2.28 2.39 6.139 6.89 6.90 7.62	05-10 PCT 78.12 17.23 2.07 1.29 .30 .20 06-10 08 3.81 3.13 2.51 2.68 1.37 1.02 .65 .62 .89 .80 -83 -83 -83 -83 -83 -83 -83 -83 -83 -83
K=4,9  SI PCT 00-19 75.2 20-39 13.5 40-59 2.6 60-79 2.6 80-89 1.1 90-99 2.2  PCT 08 .05 6.7 .10 5.6 .20 4.56 .2	CI(  18-14  93.J1  5.72  1.J3  6.J0  0.00  18-14  2.27  1.88  1.52  1.39  1.15  1.56  1.56  1.57  1.58  1.59  1.59  1.59  1.50	JRNAL VAP 14-18 90-26 70-72 20-25 -63 -67 JRNAL VAR 14-18 14	IATION  18-22 FCT  79.05 10.79 4.29 2.46 2.46 2.46 IATION 18-22 X CB 6.62 5.68 4.61 3.23 2.22 1.42 .68 .32 -02 6.00 -02 6.00 -02 -03 -02 -03 -02 -03 -02 -03 -02	2 PC 543	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 82-86 3.59 5.57 4.22 3.28 2.28 1.39 .75 .36 .18 .86 8.80 14 33 46 268 379	06-10 PCT 78.12 17.23 2.87 1.29 .30 .20 06-10 x 3.81 3.13 2.51 1.37 1.82 .65 .42 .83 .83 .83 .83 .83 .83 .83 .83 .83 .83
K=4.9   80-2   SI	CI(  18-14  93. J1  5. 72  1. J3  6. J0  9. 30  10-14  X	URNAL VAP 14-16 99.26 7.72 2.26 .63 .07 .67  URNAL VAR 14-18 1.04 1.04 1.04 .73 .41 .27 .89 .81 8.08 .51 4.08 .73 .73 .73 .73 .73 .73 .73 .73	IATION  18-22 FCT 79.05 10.79 4.29 2.4695 2.46 IATION 18-22 X CB 6.62 5.66 4.61 3.23 2.22 1.42030303030303030	2 PC 5 4 3 7 - 1 5 5 5 1 2 PC 5 4 - 5 1 5 5 1 2 PC 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5	02-06 PCT 53.15 21.59 6.86 2.15 4.45 82-06 X DB 5 6.69 5.57 4.22 3.28 2.28 1.39 .75 .36 .18 .06 8.00 85 33 33 33 33 33 33 33 3	05-10 PGT 78.12 17.23 2.07 1.29 .20 .20 .20 .20 .20 .20 .20 .20 .20 .20
K=4,9  SI PCT 00-19 75.2 20-39 13.5 40-59 2.6 60-79 2.6 80-89 1.1 90-99 2.2  PCT 08 .05 6.7 .10 5.6 .20 4.56 .2	CI(  18-14  93. J1  5. 72  1. J3  9. J0  18-14  20. 27  1. 88  1. 52  1. 81  1. 52  1. 81  1. 92  1. 93  1. 93  1. 93  1. 93  1. 94  1.	JRNAL VAP 14-18 90-26 70-72 20-25 -63 -67 JRNAL VAR 14-18 14	IATION  18-22 FCT  79.05 10.79 4.29 2.46 2.46 2.46 IATION 18-22 X CB 6.62 5.68 4.61 3.23 2.22 1.42 .68 .32 -02 6.00 -02 6.00 -02 -03 -02 -03 -02 -03 -02 -03 -02	2 PC 543	02-06 PCT 53.15 21.59 12.59 6.86 2.15 4.45 82-86 3.59 5.57 4.22 3.28 2.28 1.39 .75 .36 .18 .86 8.80 14 33 46 268 379	06-10 PCT 78.12 17.23 2.87 1.29 .30 .20 06-10 x 3.81 3.13 2.51 1.37 1.82 .65 .42 .83 .83 .83 .83 .83 .83 .83 .83 .83 .83

		AT	S <b>-3</b>	NOV-J	AN	1964-72	L	CCAL TIME
K=0-3	•		CIU	RNAL VARI	ATION			
	00-24		10-14	14-18	10-22	22-02	82-86	06-10 PCT 51.84 27.52 12.85 5.68 1.61
SI	PCT		PCT	PCT	PCT	PCT	PC1	PCT
98-19	35.83		41.74	29.15	33.29	23.65	35.78	51.04
48-59	16.32		13.51	20.70 18.51	19.41	18.58	27.38 15.43	12.45
68-79	9.22		6.89	11.70	6, 93	12.01	18.83	5.68
81-89	3.94		2.66	5.00	3.00	5.81	5.54	1.61
98-99	5.32		3.31	7.08	3.30	9.36	7.63	1.30
	18-24		10-14	14-18	18-22	25-65	12-16	06-10
PCT	98	X	DB X	08 X	98	X CB	X DB	X 08 X
-10	7.62		7.37 6.32	8.03 B	7.41	7.56	8 8.85	B 6.13
.28	5.94		5.22	6.39	5.26	6-82	6.50	4.28
.50	4.54		3.76	4.94	4.84	5.32	5.04	3.13
1.00	3.68		3.03	3.98	3.15	4.32	4.16	2.41
2.88	2.65		2.21	Z.99	2.36	3.29	3.14	1.79
18.80	. 99		- 14	1.16	1.46	1.25	1.00	1112
20.03	.49		.42	.51	.58	.63	.52	.35
30.88	.25		.21	.29	.26	.32	.26	-16
45.88	-10		. 19	.12	-11	.13	.10	. 87
50.00	0.42		0. 10 - 18	0.00 0.12	5. EU	0.13	0.00	8488 - 67
78.00	25		21	38	25	33	25	-417
31.88	51		43	61	52	67	53	~.34
90.00	-1.08		31	-1.26	-1.05	-1.39	-1.20	75
95.88	-1.53		-1.53	-2.89	-1.78	-2.38	-2.88	-1.26
99.00	-5.34		~2.75 -3.56	-3.52	-2.75	-3.72	-3.77	-2.89 -2.89
99.58	-5.85		-1.34	-5.58	-4.93	-7.29	-6.78	-3.74
99.48	-8.31		-7.37	-9.96	-7.12	-9.44	-9.28	-5.15
99.90	-10.26	_	-8.91	-11.14	-8.94	-12.19	-11.43	-6.78
79.95	-12.39	Э.	-19.33	-13.94	-18.94	-15.14	A -14.45	-8.46
NARSSA	RSSUAQ	AT	S-3	FCi	FŔ	1964-72	L	06-10 X 08 X 6.13 5.05 4.29 3.13 2.41 1.79 1.12 .76 .35 .107 0.98 07 34 75 -1.26 -2.09 -2.09 -2.09 -3.74 -5.15 -6.70 -6.76 -6.76
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K=8-3	}							06-18 PCT 42-13 32-67 13-1 6-6 2-3
K=8-3	80-24 PCT 24.15 22.72 14.77 11.70 6.78		EIU 18-14 PCT 907 32-36 32-39 13-49 4-57 1-21 2-18	RNAL VARI 14-18 PCT 28.89 29.62 17.95 11.14 4.65 6.34	ATION 18-22 PCT 9.41 13.38 15.09 14.72 11.00 36.40	22-82 PGT 5.31 6.85 12.48 16.51 11.66 45.18	02-06 PCT 11.38 18.69 16.65 17.63 18.30 25.64	96-18 PCT 42-13 32-67 13-1 6-6 2-7
SI 84-19 28-39 48-59 68-79 88-89 98-99	80-24 PCT 24-15 22-72 14-77 11-70 6-78 19-89		EIU 18-14 PCT 45-36 32-69 13-49 4-57 1-21 2-18	RNAL VARI 11-18 9CT 28-89 29-62 17-95 11-14 4-65 6-34 RNAL VARI	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION	22-82 PCT 5.31 6.85 12.48 16.51 11.66 45.18	82-86 PCT 11.38 18.69 16.65 17.83 18.39 25.84	96-18 PCT 42-13 32-67 13-1 6-9 2-3-18
SI 98-19 28-39 48-79 68-79 99-99	80-24 PCT 24-15 22-72 14-77 11-70 6-78 19-89		EIU 18-14 PCT 45-36 32-69 13-49 4-57 1-21 2-18	RNAL VARI 11-18 9CT 28-89 29-62 17-95 11-14 4-65 6-34 RNAL VARI	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION	22-82 PCT 5.31 6.85 12.48 16.51 11.66 45.18	82-86 PCT 11.38 18.69 16.65 17.83 18.39 25.84	96-18 PCT 42-13 32-67 13-1 6-9 2-3-18
K=8-3 SI 08-19 28-39 48-59 68-79 88-89 98-99	80-24 PCT 24-15 22-72 14-77 11-78 6-78 19-89 80-24 DB 7-15	X B	CIU 18-14 PCT 45-36 32-69 13-49 4-57 1-21 2-18 0IU 10-14 CB X 6-35	RNAL VARI 11-18 PCT 28-89 29-62 17-95 11-14 4-65 8-34 RNAL VARI 14-18 DB X 6-13 B	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.80 36.48 ATION 18-22 DB 6.67	22-02 PCT 5.31 6.05 12.44 16.51 11.66 45.10	02-06 PCT 11.38 10.00 16.65 17.03 18.30 25.84 02-06 X DB 8 7.21	96-18 PCT 42-13 32-67 13-1 6-6 2-7
SI 88-19 28-39 48-59 68-79 88-89 90-99 PCT •85 •10 •28	80-24 PCT 24.15 22.72 14.77 11.78 6.78 19.89	X B	ETU 18-14 PCT 45-36 32-69 13-49 1-21 2-18 010 10-14 CB X 5-53 4-30	RNAL VARI 14-18 PCT 24.89 29.62 17.95 11-14 4.65 8.34 RNAL VARI 14-18 DB X 6.13 B 7.55 6.66	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 DB 6.67 7.51 8.21	22-02 PCT 5.31 5.45 12.46 16.51 11.66 45.18 22-02 X D8 8 6.13 8 7.78 8 8.07	82-86 PCT 11.38 18.68 16.65 17.03 18.30 25.84 02-86 X DB 8 7.21 8 7.21 8 7.94	96-18 PCT 42-13 32-67 13-1 6-4 2-3-3 3-16 86-19 X On X 8 7-28
X=8-3 SI 88-19 28-39 48-79 68-79 98-99 PCT •85 •10 •28 •58	80-24 PCT 24.15 22.72 14.77 11.77 6.78 19.89 80-24 DB 7.15 8.04 7.46	X B	ETU 18-14 PCT 45.36 32.69 13.49 1.21 2.18 10-14 X 6.65 5.33 4.30	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 08 X 6.13 B 7.55 6.60 9.13	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 D8 6.67 7.51 8.21 7.31	22-82 PCT 5.31 5.45 12.48 14.51 11.66 45.18 22-82 X D8 8 6.13 8 7.78 8 8.67 7.55	02-06 PCT 11.38 18.69 16.65 17.03 18.30 25.84 02-06 X DB 7.21 8 7.21 8 7.94 6.87	96-18 PCT 42-13 32-67 13-1 6-4 2-5. 3-18 86-19 X On X 8 7-28 6-21 5-11 3-87
X=8-3 SI 08-19 28-39 48-59 68-89 90-99 PCI •85 •10 •28	80-24 PCT 24.15 22.72 14.77 6.78 19.89 88-24 DB 7.15 8.04 7.68 6.31	X B	GIU 18-14 PCT 45.36 32.69 13.49 4.57 1.21 2.18 10-14 X 6.65 5.53 4.50 2.52	RNAL VARI 14-18 9CT 28-89 29-62 17-95 11-14 4-65 6-34 RNAL VARI 14-18 08 X 6-13 B 7-55 6-60 5-13	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 D8 6.67 7.51 8.21 7.31 6.26	22-02 PCT 5.31 -0.45 12.48 14.51 11.66 45.10 22-02 X 08 6.13 8 6.13 8 7.78 8 8.67	02-06 PCT 11.38 10.69 16.65 17.03 25.84 02-06 X 08 8 7.21 8 7.96 8 7.97	96-18 PCT 42-13 32-67 13-1 6-6 2-5 3-10 86-18 X Ob X 8 7-26 8 6-21 5-11 3-47 2-95
X=8-3 SI 88-19 28-39 48-79 68-79 98-99 PCT •85 •10 •28 •58	80-24 PCT 24.15 22.72 14.77 11.78 19.89 80-24 7.15 8.04 7.68 6.42 5.31	X B	GIU 18-14 PCT 45.36 32.69 13.49 4.57 1.21 2.18 0.10 10-14 X 6.85 5.33 4.30 3.32 2.32 1.85	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 08 X 6.13 B 7.55 6.60 9.13	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.80 36.48 ATION 18-22 D8 6.67 7.51 8.21 7.31 6.26 5.15	22-02 PCT 5.31 6.05 12.48 16.51 11.64 45.10 22-02 X 06.13 8 6.13 8 7.70 8 8.07 7.55 5.40	02-06 PCT 11.38 10.65 17.03 18.30 25.84 02-06 X 08 7.21 8 7.96 6.87 5.75 4.66	06-18 PCT 42-13 32-67 13-1 6-6 2-3-3 3-18 06-19 X On X 8 7-28 8 6-21 5-31 3-87 2-95 2-14
X=8-3 SI 08-19 28-39 48-59 68-79 88-89 98-99 PCI -85 -10 -28 -58 1-88 2-86	80-24 PCT 24.15 22.72 14.77 16.78 19.89 80-24 DB 7.15 8.04 5.31 4.27 2.76 4.27 2.76	X B	GIU 18-14 PCT 45.36 32.69 13.49 4.57 1.21 2.18 10-14 X 6.65 5.53 4.50 2.52	RNAL VARI 11-18 PCT 28-89 29-62 17-95 11-14 4-65 6-34 RNAL VARI 14-18 DB X 6-13 B 7-55 C-60 5-13 4-15 3-11	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 D8 6.67 7.51 8.21 7.31 6.26	22-02 PCT 5.31 -0.45 12.48 14.51 11.66 45.10 22-02 X 08 6.13 8 6.13 8 7.78 8 8.67	02-06 PCT 11.38 10.69 16.65 17.03 25.84 02-06 X 08 8 7.21 8 7.96 8 7.97	96-18 PCT 42-13 32-67 13-1 6-6 2-5 3-10 86-18 X Ob X 8 7-26 8 6-21 5-11 3-47 2-95
X = 8 - 3 SI = 9 28 - 39 48 - 79 50 - 89 90 - 99 PC T = 5 • 10 80 2.80 10 80 20 80 20 80	80-24 PCT 24.15 22.72 14.77 11.78 6.78 19.89 80-24 7.15 8.84 7.642 5.31 4.27 2.75 1.75	X B	18-14 45.36 92.69 13.57 1.21 10-14 X 6.65 3.32 1.85 1.15 	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 8.13 B 7.55 6.60 9.13 4.15 3.11 1.89 1.69	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 08 6.67 7.51 6.26 5.15 3.72 2.99 1.27	22-82 PCT 5.31 5.45 12.48 14.51 11.66 45.18 22-82 X DB 6.13 B 6.13 B 7.78 6.58 5.48 4.83 1.54	02-06 PCT 11.38 10.65 17.03 10.39 25.84 02-06 X 08 8 7.21 7.06 8 7.21 8 7.96 6.07 5.75 4.66 3.22 1.64	96-18 PCT 42.13 32.67 13.1 6.6 2.5. 3.18 86-19 X On X B 7.26 8 6.21 5.11 3.87 2.95 2.14 1.31
X=8-3 SI 98-19 28-39 48-79 58-89 90-99 PC 10 -28 -10 20 20 20 20 38-08	80-24 PCT 24.15 22.72 14.77 6.78 19.89 88-24 7.15 8.04 7.68 6.31 4.27 2.75 1.64 7.53	X B	GIU 18-14 45.36 32.69 13.49 1.21 2.08 10-14 X 6.65 5.33 4.30 2.32 1.85 1.16 2.20	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 8.13 B 6.13 B 6.13 B 6.13 B 7.55 6.60 3.13 4.15 3.11 1.89 1.16 .57	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 08 6.67 7.51 6.21 7.31 6.26 5.15 3.72 2.49	22-82 PCT 5.31 -0.45 12.48 14.51 11.66 45.18 22-82 X DB 6.13 8 6.13 8 7.78 8 6.93 6.58 5.44 4.86 2.63 1.54	02-06 PCT 11.38 10.69 17.03 25.84 02-06 X 08 7.21 9 7.96 8 7.97 4.66 3.22 2.07 1.64	96-18 PCT 42-13 32-67 13-1 6-6 2-3-3 3-10 86-19 X Ob X 8 7-26 8 6-21 5-11 3-47 2-95 2-14 1-31
X = 8 - 3 SI - 19 28 - 39 48 - 79 88 - 89 90 - 99 PC T - 28 - 28 - 28 1 - 80 1 - 80 2 - 80 1 - 80 2 - 80 2 - 80 2 - 80 2 - 80 3 - 80 3 - 80 3 - 80 3 - 80 3 - 80 3 - 80	80-24 PCT 24.15 22.72 14.77 11.78 6.78 19.89 80-24 DB 7.15 8.04 7.68 6.42 5.31 4.27 2.75 1.64	X B	ETU 18-14 45.36 32.69 4.21 2.08 4.21 2.08 5.53 2.32 2.38 2.32 2.38 2.32 2.38 3.32 2.38 3.32 2.38 3.32 2.38	RNAL VARI 1'-18 PCT 24.89 29.62 17.95 11.14 4.65 8.34 RNAL VARI 14-18 DB X 6.13 B 7.55 6.60 5.13 4.15 3.11 1.89 1.16 .57 .29 .12	ATION 18-22 PCT 9.41 13.38 15.98 14.72 11.88 36.48 ATION 18-22 D8 6.67 7.51 6.21 7.31 6.26 5.15 3.72 2.49 1.27	22-82 PCT 5.31 6.45 14.51 11.66 45.18 22-82 X DB 6.13 8 6.13 8 6.13 8 6.54 4.86 2.23 1.54	82-86 PCT 11.38 18.89 16.65 17.03 18.30 25.84 82-86 X 7.21 7.21 7.26 8 7.27 5.75 4.66 3.22 2.07 1.64 .53	96-18 PCT 42-13 32-67 13-1 2-5 3-18 96-19 X 7-26 8 6-21 5-11 3-47 2-95 2-14 1-31 -02 -41 -88
X=8-3 SI 98-19 28-39 48-79 58-89 90-99 PC 10 -28 -10 20 20 20 20 38-08	80-24 PCT 24.15 22.72 14.77 6.78 19.89 88-24 7.15 8.04 7.68 6.31 4.27 2.75 1.64 7.53	X B	GIU 18-14 45.36 32.69 13.49 1.21 2.08 10-14 X 6.65 5.33 4.30 2.32 1.85 1.16 2.20	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 8.13 B 6.13 B 6.13 B 6.13 B 7.55 6.60 3.13 4.15 3.11 1.89 1.16 .57	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 08 6.67 7.51 6.21 7.31 6.26 5.15 3.72 2.49	22-82 PCT 5.31 -0.45 12.48 14.51 11.66 45.18 22-82 X DB 6.13 8 6.13 8 7.78 8 6.93 6.58 5.44 4.86 2.63 1.54	02-06 PCT 11.38 10.69 17.03 25.84 02-06 X 08 7.21 9 7.96 8 7.97 4.66 3.22 2.07 1.64	96-18 PCT 42-13 32-67 13-1 6-6 2-3-3 3-10 86-19 X Ob X 8 7-26 8 6-21 5-11 3-47 2-95 2-14 1-31
X = 8 - 3 SI - 19 28 - 39 48 - 79 58 - 79 90 - 9 PC 185 - 10 - 28 1 - 80 2 - 80 2 - 80 3 - 80 3 - 80 5 - 80 5 - 80 5 - 80 5 - 80 5 - 80 6 - 80 7 - 80 6 - 80 7 - 80 6 - 80 7 - 80 6 - 80 6 - 80 7 - 80 6 - 80 7 - 80 8 -	80-24 PCT 24.15 22.72 14.77 6.78 19.89 80-24 7.15 8.04 7.682 5.31 4.27 2.75 1.642 9.36 9.36 9.36 9.36 9.36 9.36	X B	TO THE TOTAL TO THE TOTAL THE T	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 X 6.13 B 6.13 B 6.13 B 6.13 B 1.89 1.15 3.11 1.89 1.16 .57 .29 .12	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 08 6.67 7.51 8.21 7.31 6.26 5.15 3.72 2.49 1.27 8.88 -27	22-02 PCT 5.31 5.45 12.48 14.51 15.66 45.10 22-02 X 08 6.13 8 6.13 8 8.07 7.78 8 8.07 1.54 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 2.154 4.06 4	02-06 PCT 11.38 10.69 16.65 17.03 18.30 25.84 02-06 X 08 7.21 8 7.86 3.22 2.07 1.64 .53 .22 2.06	96-18 PCT 42.13 32.67 13.1 6.5 2.5 3.10 86-18 X On X 8 6.21 5.31 3.47 2.95 2.14 1.31 .02 .41 .21
X = 8 - 3 SI - 19 28 - 359 68 - 769 68 - 89 90 - 9 P G T 55 • 28 • 28 • 28 10 - 80 10 - 80 50 - 80 10 - 80 50 - 80 68 - 80	80-24 PCT 24.15 22.72 14.77 11.78 6.78 19.89 80-24 DB 7.15 8.04 7.68 6.42 7.68 6.42 7.64 9.37 9.37 9.37 9.37 9.38	X B	ETU 18-14 45.36 45.3	RNAL VARI 14-18 PCT 24-89 29-62 17-95 11-14 4-65 8-34 RNAL VARI 14-18 DB X 6-13 6-13 6-13 1-15 3-11 1-89 1-16 -57 -29 -12 -38 -68	ATION 18-22 PCT 9.41 13.38 15.98 14.72 11.88 36.48 ATION 18-22 D8 6.67 7.51 6.21 7.31 6.26 5.15 3.72 2.49 1.2/ 6.86 -1.38	2-02 PCT 5.31 5.45 14.51 11.66 45.18 22-02 X 08 6.13 7.55 6.54 4.06 2.23 1.54 4.06 2.23 1.54	02-06 PCT 11.38 18.89 16.89 17.03 18.30 25.84 02-06 X 7.21 7.21 8 7.21 8 7.94 6.87 5.75 4.66 3.22 2.07 1.64 .53 .22 2.07	06-18 PCT 42-13 32-67 13-1 6.6 2.5. 3-10 86-10 X 7-26 8 6-21 5-11 3-87 2-95 2-14 1-31 -02 -01 -08 8-00 -08 8-00
X = 8 - 3 SI - 19 28 - 39 68 - 79 88 - 79 88 - 79 90 - 9 P C 15 - 12 - 12 - 13 - 13 - 14 - 15 - 16 - 16 - 18 - 18 - 18 - 18 - 18 - 18 - 18 - 18	80-24 PCT 24.15 22.72 14.77 16.78 19.89 80-24 DB 7.15 8.04 7.15 8.04 7.16 9.31 4.27 1.64 75 75 34 36 36 36	X B	TO THE PROPERTY OF THE PROPERT	RNAL VARI 10-18 PCT 28.89 29.62 17.95 11.14 4.65 8.34 RNAL VARI 14-18 DB X 8.13 B 7.55 6.60 5.13 4.15 3.11 1.89 1.16 .57 .29 .12 8.00 12 8.00 12 8.13 8.15	ATION 18-22 PCT 9:41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 DB 6.67 7.51 6.26 5.15 2.49 1.27 .68 -27 -68 -27	2-02 PCT 5.31 5.45 12.48 11.66 45.18 22-02 X D8 3 8 6.13 7.78 8 8.07 7.55 6.54 4.46 2.23 1.54 1.54 1.54 1.54 1.54	82-86 PCT 11.38 18.88 16.65 17.03 18.30 25.84 8 7.21 8 7.94 6.87 5.75 4.66 3.22 2.07 1.64 .53 2.10 1.64 .53 1.22 2.10 1.64 .53 1.64 1.64 1.64 1.64 1.64 1.64 1.64 1.64	06-18 PCT 42-13 32-67 13-1 6-4 2-5 3-18 06-10 X On X 8 7-28 8 6-21 5-21 3-87 2-95 2-14 1-32 -41 -21 -21 -21 -21 -21 -21 -21 -21 -21 -2
X = 8 - 3 SI - 19 28 - 39 48 - 79 58 - 79 99 - 9 P C T 5 - 10 8 - 28 8 10 8 8 28 - 88 28 -	80-24 PCT 24.15 22.77 11.78 6.78 19.89 80-24 19.89 7.15 8.04 6.42 5.31 4.27 2.75 3.64 6.42 6.42 6.42 6.44 6.42 6.44 6.44 6	X B	TO THE PROPERTY OF THE PROPERT	RNAL VARI 10-18 PCT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 28.13 8.13 8.13 8.13 8.13 8.13 14-18 9.10 1.16 .57 .29 .12 9.00 -12 -38 -1.28 -1.28 -2.15	ATION 18-22 PCT 9:41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 DB 6.67 7.51 6.26 5.15 3.79 1.27 8.882768 -1.382768	2-02 PCT 5.31 5.45 12.48 11.66 45.18 22-02 X DB 3.7.78 8 6.13 8 7.78 6.50 5.40 4.05 1.54 34 34 34 34 34	02-06 PCT 11.38 10.65 17.03 10.30 25.84 02-06 X DB 7.26 7.94 6.87 5.75 4.62 2.07 1.64 .53 .22 4.08 22 56	96-18 PCT 42.13 32.67 13.1 6.4 2.5.3 3.18 86-19 X On 8 6.21 5.11 3.87 2.95 2.14 1.31 .02 .41 .21 .02 .41 .21 .02 .41
X SI-199 88-399 88-399 88-7899 98-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889 12-889	80-24 PCT 24.15 22.72 14.77 11.78 6.78 19.89 80-24 DB 7.16 8.94 7.68 6.42 7.68 6.42 7.64 9.37 9.37 9.37 9.37 9.38 9.31 9.31 9.33 9.33 9.33 9.33 9.33 9.33	X B	ETU	RNAL VARI 10-18 PCT 28.89 29.62 17.95 11.14 4.65 8.34 RNAL VARI 14-18 DB X 8.13 B 7.55 6.60 5.13 4.15 3.11 1.89 1.16 .57 .29 .12 8.00 12 8.00 12 8.13 8.15	ATION 18-22 PCT 9:41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 DB 6.67 7.51 6.26 5.15 2.49 1.27 .68 -27 -68 -27	2-02 PCT 5.31 5.45 14.51 11.66 45.18 2-02 X 08 6.13 7.55 6.54 4.06 2.23 1.54 -3.4 -3.4 -3.4 -3.4 -3.6 -3.21 -5.65 -3.21	82-86 PCT 11.38 18.88 16.65 17.03 18.30 25.84 8 7.21 8 7.94 6.87 5.75 4.66 3.22 2.07 1.64 .53 2.10 1.64 .53 1.22 2.10 1.64 .53 1.64 1.64 1.64 1.64 1.64 1.64 1.64 1.64	06-18 PCT 42-13 32-67 13-1 6-4 2-5 3-18 06-10 X On X 8 7-28 8 6-21 5-21 3-87 2-95 2-14 1-32 -41 -21 -21 -21 -21 -21 -21 -21 -21 -21 -2
X = 8 - 9 88 - 19 28 - 39 48 - 79 48 - 79 48 - 79 90 - 99 90 - 99 12 - 80 13 - 80 14 - 80 18 - 80 1	80-24 PCT 24.15 22.72 14.77 16.78 19.89 80-24 DB 7.15 8.04 7.68 6.42 9.31 4.27 1.64 16 16 16 16 16 16 16 16	X B	ET	RNAL VARI 10-18 PCT 28.89 29.62 17.95 11.14 4.65 8.34 RNAL VARI 14-18 DB X 8.13 B 7.55 6.60 5.13 4.15 3.11 1.89 1.16 .57 .29 .12 8.00 -12 8.00 -12 -3.15 -3.67 -5.13 -6.95	ATION 18-22 PCT 9.41 13.38 15.89 14.72 11.88 36.48 ATION 18-22 DB 6.67 7.31 6.26 5.17 2.49 1.2768 -2.7698 -1.38 -1.16	2-02 PCT 5.31 5.45 12.45 12.46 14.51 11.66 45.18 22-02 X D8 3 8 6.13 7.78 8 8.07 7.55 6.54 4.46 2.63 1.54 -3.4 -3.4 -3.6 -3.6 -3.6 -3.6 -3.6 -3.6 -3.6 -3.6	82-86 PCT 11.38 18.88 16.65 17.83 18.30 25.84 8 7.21 8 7.94 6.87 5.75 4.66 3.22 2.07 1.64 .53 2.20 1.64 .53 -22 -3.80 -6.87 -11.27	06-18 PCT 42-13 32-67 13-1 6-4 2.5.3 3-18 06-10 X On 2 6-21 5-21 3-87 2-95 2-14 1-02 -21 -21 -21 -21 -21 -21 -21 -21 -21 -2
X = 8 - 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	80-24 PCT 24.15 22.77 14.78 19.89 19.89 80-24 19.89 7.15 8.04 7.68 5.31 4.27 2.75 .36 -1.82 -3.13 -5.36 -7.31 -7.31	X B	ET	RNAL VARI 10-18 26.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 10-18 8.13 8.	ATION  18-22  9:41  13.38  15.89  14.72  11.88  36.48  ATION  22  DB  6.67  7.51  6.26  5.17  2.49  1.27  -68  -1.38  -7.83  -4.51  -7.83  -1.16  -15.15	2-02 PCT 5.31 6.45 12.48 11.66 45.18 22-02 X DB 3 7.78 8 6.13 8 7.78 6.50 5.40 4.63 1.54 34 34 34 34 34 34 34 3	02-06 PCT 11.38 16.65 17.03 10.30 25.84 02-06 X DB 7.26 8 7.26 8 7.26 0.87 5.75 4.68 3.22 2.07 1.64 .53 2.20 1.64 .53 2.20 1.64 .53 2.20 1.64 .53 2.20 1.64 .53 2.20 1.64 .53 2.20 1.64 .53 2.20 1.64 .53 1.64 1.64 1.64 1.64 1.64 1.64 1.64 1.64	96-18 PCT 42.13 32.67 13.16 2.5.3 3.18 86-18 X On 28 6.21 3.87 2.95 2.14 1.31 .02 .01 .02 .01 .02 .041 .02 .041 .02 .041 .02 .041 .02 .041 .02 .041 .02 .041 .041 .041 .041 .044 .044 .044 .044
X SE-39 98-39 98-39 98-39 98-39 98-39 98-38 108	80-24 PCT 24.15 24.15 22.77 11.78 6.78 19.89 80-24 19.89 7.15 8.04 7.42 5.31 4.27 2.75 4.27 2.75 4.27 3.36 -1.82 -	X 8 8	ETU	RNAL VARI 14-18 9CT 28.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 14-18 8.13 8.13 7.55 6.60 5.13 4.15 3.11 1.89 1.16 .57 .29 .12 8.20 8.38 -1.28 -2.15 -3.67 -9.13 -9.13	ATION 18-22 9:41 13.38 15.89 14.72 11.88 36.48 ATION 22 6.67 7.51 7.31 6.26 5.15 3.749 1.2768 -1.38 -2.79 -7.83 -4.94 -11.16 -15.15 3.10	22-02 PCT 5.31 5.45 12.48 11.66 45.18 22-02 X D8 6.13 8 6.13 8 6.13 8 7.78 6.58 4.03 4.03 -20 -1.54 -1.55 -1.54 -1	02-06 PCT 11.38 10.65 17.03 10.30 25.84 02-06 X 7.21 7.06 X 7.21 8 7.96 5.75 4.66 3.22 2.07 1.64 .53 .22 4.08 -1.12 -2.32 -1.12 -2.32 -1.1	96-18 PCT 42.13 32.67 13.1 6.5 3.18 86-18 X Du Z6 6.21 3.47 2.95 2.14 1.32 .21 .21 .21 .21 .21 .21 .21 .21 .21 .2
X = 8 - 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	80-24 PCT 24.15 22.77 14.78 19.89 19.89 80-24 19.89 7.15 8.04 7.68 5.31 4.27 2.75 .36 -1.82 -3.13 -5.36 -7.31 -7.31	X 8 8	ET	RNAL VARI 10-18 26.89 29.62 17.95 11.14 4.65 6.34 RNAL VARI 10-18 8.13 8.	ATION 18-22 9:41 13.38 15.89 14.72 11.88 36.48 ATION 22 6.67 7.51 7.31 6.26 5.15 3.749 1.2768 -1.38 -2.79 -7.83 -4.94 -11.16 -15.15 3.10	2-02 PCT 5.31 6.45 12.48 11.66 45.18 22-02 X DB 3 7.78 8 6.13 8 7.78 6.50 5.40 4.63 1.54 34 34 34 34 34 34 34 3	02-06 PCT 11.38 10.65 17.03 10.30 25.84 02-06 X 7.21 7.06 X 7.21 8 7.96 5.75 4.66 3.22 2.07 1.64 .53 .22 4.08 -1.12 -2.32 -1.12 -2.32 -1.1	96-18 PCT 42.13 32.67 13.16 2.5.3 3.18 86-18 X On 28 6.21 3.87 2.95 2.14 1.31 .02 .01 .02 .01 .02 .041 .02 .041 .02 .041 .02 .041 .02 .041 .02 .041 .02 .041 .041 .041 .041 .044 .044 .044 .044

NARSSA K=0-3	RSSUAQ	AT	S-3	L-YAH	UL	1	968-72		LO	CAL	. TIME	
V=#-0			DIUF	RHAL VARI	ATION							
	00-24		10-14	14-18	18-22		55-05		02~06		06-10	
SI	PCT		PCT	PCT	PCT		PCT		PCT		PCT	
00-19 20-39	34.56 21.22		64.47 27.43	51.32 28.16	13.78 17.92		3.76 6.60		13.75 22.43		59.50 24.78	
40-59	12.87		6.38		16.97		10.91		22.85		8.19	
	10.65		.89	4.49	17.29				18.37		4.56	
	6.99		. 34	1.71	10.60		18.57		9.63		1.35	
90-99	13.72		. 48	2.09	23.25		41.93		12.98		1.62	
			DIU	RNAL VARI	ATION							
	00-24		10-14	14-18	18-22		55-05		02-06		06-18	
PCT	<b>0</b> B		DB X	CB X				X	08		09 X	
.05	7.71 8.00	В	4.42 3.59	6.72 5.59	6.5i 7.93		6.06 7.11		7.56 7.97	В	6.33 5.22	
.20	7.29		2.90	4.56	7.85	0	8.05		7.30		4.29	
.50	5.88		2.12	3.37	6.71		7.50	•	5.89		3.12	
1.00	4.79		1.64	2.55	5.60		6.52		4.81		2.33	
2.00	3.17		1,24	1.85	4.53		5.41		3.84		1.67	
5.00 10.00	2.30 1.34		.52 .52 .27	1.14 .70	3.10 1.98		4.01 2.82		2.50 1.60		1.01	
20.00	.59		.27	•70 •35	.94		1.59		. 84		.32	
33.00	. 25			.17	.51		.86 .37 0.00		.44		.14 .05 0.00	
48.00	.10 0.00		.06 0.36	0.00	.21 0.09		.37		.19		.05	
	0.80 10				0.09 21		0.00 38		9.98		0.00 - 85	
70.00			12	17 34 75	53		50		46		05 12 27	
	~.60		12 23	34	-1.06		90 -1.72		-,90		27	
	-1.47		51	75	-2.21		-3.23		-1.79		62	
	-2.60		58	-1.25	-3.63		-4.98		-1.79 -2.86 -4.68 -6.34 -8.23		-1.11	
	-4.58 -6.33		-1.47 -1.39	-2.17 -2.98	-5.85 -7.80		-1.49		-4.50		-1.95 -2.70	
99.50	-8.28		-2.53	-4.06	-9.77		-11.78		-8.23		-3.71	
99.80	-8.28 -10.98		-3.50	-5.87	-12.66		-14.74	8	-10.85		-5.33	
99.98	-13.73		-4.35	-7.70			23.48	В	-13.25		-/.45	
99.95	-10.11		-5.61	-9.57	23.11	8	119.97	B	-11.63	9	-8.57	
	APSSUAG	<b>A</b> 1	TS-3	AUS-C	CT	;	1968-72		L	CA	L TIME	
NARSS K=Q-		<b>A</b> 1			-	;	1968-72		L	CA	L TIME	
K=Q	3 00-24		CIU 10-14	PHAL VARI	ATION	;	1 <b>968-</b> 72 22 <b>-0</b> 2		02-06 L(	CA	06-10	
K=0	3 00-24 PCT		CIU 10-14 PCT	PNAL VARI 14-18 FCT	ATION 16-22 FCT		22-02 PC1		02-06 PCT	)CA	96-10 PCT	
%=0 SI 00-19	3 00-24 PCT 34.36		CIU 10-14 PCT 53-58	PHAL VARI 14-18 FCT 46-63	ATION 16-22 FCT 16.38		22-82 PCT 7-19		02-06 PCT 23.16	)CA	06-10 PCT 59-52	
K=0	3 00-24 PCT 34.36 23.03	1	CIU 10-14 PCT 53-58 27-12	FHAL VAR 14-18 FCT 46-63 26-60	ATION 16-22 FCT 16.38 16.83		22-02 PCT 7.19 15.24		02-06 PCT 23.16 27.28	CA	06-10 PCT 59.52 24.79	
SI 00-19 20-39 40-59 <b>68-</b> 79	3 00-24 PCT 34.36 23.03 16.31 11.75	•	CIU 10-14 PCT 53-58 27-12 10-39	PHAL VARI 14-18 FCT 46-63	ATION 16-22 FCT 16.38		22-82 PCT 7-19		02-06 PCT 23.16	CA	06-10 PCT 59-52	
X=0 SI 00-19 20-39 40-59 68-79	3 00-24 PCT 34.36 23.03 16.31 11.75	•	CIU 18-14 PCT 53.58 27.12 10.39 4.57	PNAL VAR 14-18 FCT 46-63 26-60 12-55 8-43 3-27	ATION 16-22 FCT 16.38 16.83 19.63 18.87		22-02 PCT 7-19 15-24 22-55 22-68 12-89		02-06 PCT 23.16 27.28 21.66 11.92 5.87	CA	06-10 PCT 59-52 24-79 10-40 3-92 1-05	
SI 00-19 20-39 40-59 <b>68-</b> 79	3 00-24 PCT 34.36 23.03 16.31 11.75	•	CIU 10-14 PCT 53.58 27.12 10.39	PNAL VAR 14-18 FCT 46-63 26-60 12-55 8-43 3-27	ATION 16-22 FCT 16.38 16.83 19.63		22-02 PCT 7.19 15.24 22.55 22.66		02-06 PCT 23.16 27.28 21.66 11.92	CA	06-10 PCT 59.52 24.79 10.40 3.92	
X=0 SI 00-19 20-39 40-59 68-79	3 00-24 PCT 34.36 23.03 16.31 11.75	•	10-14 PCT 53-58 27-12 10-39 4-57 1-31 1-73	PNAL VAR 14-18 FCT 46-63 26-60 12-55 8-43 3-27	16-22 FCT 16-38 16-83 19-63 18-87 11-22		22-02 PCT 7-19 15-24 22-55 22-68 12-89		02-06 PCT 23.16 27.28 21.66 11.92 5.87	DCA	06-10 PCT 59-52 24-79 10-40 3-92 1-05	
K=0- SI 00-19 20-39 40-59 68-79 88-89 98-99	3 00-24 PCT 34.36 23.03 16.31 X1.75 6.04 8.51		CIU 10-14 PCT 53-58 27-12 10-39 4-57 1-31 1-73	FHAL VARI 14-18 FCT 46-63 26-80 12-55 8-43 3-27 2-30 RNAL VARI 14-18	16-22 FCT 16-38 16-83 19-63 18-87 11-22		22-02 PCT 7-19 15-24 22-55 22-68 12-89		02-06 PCT 23.16 27.28 21.66 11.92 5.87	DCA	06-10 PCT 59-52 24-79 10-40 3-92 1-05	
K=0- SI 00-19 20-39 40-59 68-79 88-89 98-99	3 00-24 PCT 34.36 23.03 16.31 11.75 6.04 8.51	X	CIU 10-14 PCT 53.58 27.12 10.39 4.57 1.31 1.73 DIU 18-14	FNAL VARI 14-18 FCT 46-63 26-80 12-55 8-43 3-27 2-30 RNAL VARI 14-18 08	ATION 16-22 FCT 16.38 16.83 19.63 18.87 11.22 17.88 (ATION 18-22	x	22-92 PCT 7-19 15-24 22-55 22-68 12-89 19-43 22-82	×	02-06 PCT 23.16 23.16 21.66 11.92 5.07 18.11	×	06-10 PCT 59-52 24-79 10-40 3-92 1-05 -33	•
X=0- SI 19 20-39 20-39 40-59 68-79 88-89 98-99	3 00-24 PCT 34.36 23.03 16.31 11.75 6.04 8.51	X	CIU 10-14 PCT 53.58 27.12 10.39 4.57 1.31 1.73 DIU 10-14 0.50	PHAL VARI 14-18 FCT 46-63 26-80 12-55 8-43 3-27 2-30 RNAL VARI 14-18 08 7-09	ATION 10-22 FCT 16.38 16.83 19.63 19.63 10.87 11.22 17.88 ATION 18-22 10.87	X	22-82 PCT 7-19 15-24 22-55 22-66 12-89 19-43 22-82 08 6-70	X 8	02-06 PCT 23.16 27.28 21.66 11.92 5.67 18.11	×	06-10 PCT 59.52 24.79 10.40 3.92 1.05 .33	•
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98.00	-4.27		-2.13	-3.	Ú\$		-5.34		-6.43		-4.76		-2.13	
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		-	DI	URNAL.	VA	RIA	TION		-,00 16		-			
K=4,9 SI	00-24 PCT	-	0I: 10-14	URNAL 14	VA -18	RIA	TION 18-22 PCT	•	22-02 FCT		02-06 PCT		86-10 PCT	
K=4,9 SI 00-19	80-24 PCT 8.45		01: 10-14 PCT 20.66	URNAL 14- Fi 12-	VA -18 CT -61	RIA	TION 18-22 PCT 5.38	•	22-02 FCT 1.14		02-06 PCT 1.46		06-10 PCT 13.37	
SI 80-19 20-39	00-24 PCT 6.45 11.75		01: 10-14 PCT 20.66 21.76	URNAL 14 Fi 12	VA -18 CT -61	RIA	TION 18-22 PCT 5.38 9.64	,	22-02 FCT 1.14 3.66		02-06 PCT 1.46 4.98		06-10 PCT 13.37 16.23	
SI 80-19 20-39	00-24 PCT 6.45 11.75		01: 10-14 PCT 20.66 21.76	URNAL 14 Fi 12	VA -18 CT -61 -59	RIA	TION 18-22 PCT 5.38 9.64	,	22-02 FCT 1.14 3.66		02-06 PCT 1.46 4.98		06-10 PCT 13.37	
SI 80-19 20-39 40-59 60-79 88-89	00-24 PCT 8.45 11.75 14.36 16.00		01: 10-14 PCT 20-66 21-76 18:41 13-47	URNAL 14- 12- 17- 17- 15- 11-	VA -18 -59 -54 -83	RIA	TION 18-22 PCT 5.38 9.64 14.88 18.36	•	22-02 FCT 1.14 3.86 9.19 15.52		02-06 PCT 1.46 4.98 9.63 16.11		86-10 PCT 13.37 16.23 18.31 15.46	
SI 80-19 20-39 40-59 60-79	00-24 PCT 8.45 11.75 14.36 16.00		01: 10-14 PCT 20.66 21.76 18:41 13.47	URNAL 14- 12- 17- 17- 15- 11-	VA -18 -59 -54 -83	RIA	TION 18-22 PCT 5.38 9.64 14.88 18.36	•	22-02 FCT 1.14 3.86 9.19 15.52		02-06 PCT 1.46 4.98 9.63 16.11		86-10 PCT 13.37 16.23 18.31 15.46	
SI 80-19 20-39 40-59 60-79 88-89	88-24 PCT 8.45 11.75 14.36 16.00 12.26 37.18		0I: 10-14 PCT 20-66 21-76 18-41 13-47 9-30 15-38	URNAL 14 FI 12 17 17 15 11 25	VA -18 -61 -59 -54 -83 -26 -21 -21	RIA	TION 18-22 PCT 5.38 9.64 14.88 18.36 12.56 39.17	•	22-02 FCT 1.14 3.86 9.19 15.52 14.06		02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41		86-10 PCT 13.37 16.23 18.31 15.46	
SI 00-19 20-39 40-59 60-79 88-89 90-99	00-24 PCT 8.45 11.75 14.36 16.00 12.26 37.18		01: 10-14 PCT 20-66 21-76 18-41 13-47 9-30 15-38	URNAL 14- 12- 17- 17- 15- 11- 25- URNAL	VA -18 -18 -59 -54 -26 -21 -28	RIA	TION 18-22 PCT 5.38 9.64 14.88 18.36 12.56 39.17 TION 18-22	•	22-02 FCT 1.14 3.66 9.19 15.52 14.04 55.66		02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41		06-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11	
SI 00-19 20-39 40-59 60-79 80-99	00-24 PCT 6.45 11.75 14.36 16.00 12.26 37.16	x	01 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38	URNAL 14- 17- 17- 17- 15- 11- 25- URNAL 14- K OF	VA -18 -59 -54 -59 -21 -21 -21	RIA	TION 18-22 PCT 5.38 9.68 14.88 18.36 12.56 39.17 TION 18-22 DB	×	22-02 FCT 1.14 3.19 15.52 14.04 55.66	X	02-06 PCT 1.46 49 9.63 16.11 14.48 53.41	x	86-10 PCT 13.37 18.31 15.46 10.52 26.11	
SI 00-19 20-39 40-59 60-79 80-99	80-24 PCT 8.45 11.75 14.36 16.00 12.26 37.18	X 8	01 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 01 10-14 0B 7.39	URNAL 14- 14- 17- 17- 15- 11- 25- URNAL 14- X 01- B 6-	VA 18 18 18 18 18 18 18 18 18 18 18 18 18	RIA	TION 18-22 PCT 5.38 9.64 14.88 18.36 12.56 39.17 TION 18-22 DB 6.38	X	22-02 FCT 13-06 9-19 15-92 14-04 55-06 22-02 CB 5-92	X 8	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41	X	86-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11	8
SI 00-19 20-39 40-59 60-79 80-99	00-24 PCT 6.45 11.75 14.36 16.00 12.26 37.16	X 9 8	01 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38	URNAL 14- 14- 17- 17- 15- 11- 25- URNAL 14- X 01- B 6- B 7-	VA 18 18 18 18 18 18 18 18 18 18 18 18 18	RIA	TION 18-22 PCT 5.38 14.88 18.36 12.56 39.17 TION 18-22 DB 6.38	X 8 8	22-02 FCT 1.14 3.66 9.19 15.52 14.04 55.66 22-02 CB 57.41	Xas	02-06 PCT 1.46 49 9.63 16.11 14.48 53.41	XS	86-10 PCT 13.37 18.31 15.46 10.52 26.11	8
X=4,9 SI 00-19 00-39 40-79 80-49 90-99 PCT -85 -10 -20 -50	80-24 PCT 8.45 11.75 14.36 16.00 12.26 37.10 80-24 08 6.56 7.45 8.13	X 9 8	01: 10-14 PCT 20.68 21.76 18.41 13.47 9.30 15.38 DI: 10-14 DB 7.39 8.11: 7.45 6.15	URNAL 14- 12- 17- 17- 15- 11- 25- URNAL 14- K DI B G- B 7-	VA8 161 161 161 161 161 161 161 161 161 16	RIA	TION 18-22 PCT 5.38 9.64 14.86 18.36 12.56 39.17 TION 18-22 DB 6.38 7.33 7.48	X 8 8	22-02 FCT 1.14 3.86 9.19 15.92 15.92 15.96 2-02 CB 5.52 7.41 7.78	Xas	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41 02-86 0B 5.63 7.47 7.59	XS	06-10 PCT 13.37 16.23 18.34 10.52 26.11 84-10 08 7.23 7.87 7.95 5.89	8
X=4,9 SI 00-19 C0-39 40-59 60-79 80-99 PCT •85 •10 •20 •20 •50 1.90	00-24 PCT 8.45 11.75 14.36 16.00 12.26 37.16 00-24 6.56 7.45 8.13 7.45	X 9 8	01 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 01 10-14 08 7.39 8.11 7.45 5.15	URNAL 14- 12- 17- 17- 15- 11- 25- URNAL 14- K DI B 6- B 7- 7-	VA8 1619 1619 1619 1619 1619 1619 1619 161	RIA	TION 18-22 PCT 8-64 14-86 18-36 12-56 39-17 TION 18-22 DB 6-38 7-33 8-05 7-33 6-38 6-38	X 8 8	2-02 FCT 43.06 9.192 15.06 9.52 15.06 2-0 2-0 2-0 7.57 7.57 6.92	Xas	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41 02-86 08.63 7.47 7.59 7.77	XS	06-10 PCT 13.37 16.23 18.31 15.46 15.46 26.11 86-19 7.23 7.87 7.95 5.89	8
SI 00-19 20-39 40-59 60-79 80-99 PCT .85 .10 .20 .50	00-24 PCT 645 11.75 14.36 16.00 12.26 37.16 00-24 08 6.56 7.45 8.13 7.36 5.19	X 9 8	0I 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 0I 10-14 0B 7.39 8.11 7.45 6.15 5.35	URNAL 14- 14- 14- 17- 17- 17- 15- 11- 25- URNAL 14- K DE B 7- 6- 5-	VA 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RIA	TION 18-22 PCT 38-048 14-86 12-56 39-17 TION 18-22 DB 6-38 7-33 8-05 7-48 6-38 5-27	X 8 8	2-02 FC14 3.86 9.19 15.04 55.86 2.8 52 7.41 7.78 6.92 5.81	Xas	02-06 PCT 1-46 4-98 9-63 16-11 14-48 53-41 02-06 08 5-63 7-47 7-59 7-74 5-75	XS	06-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11 86-10 08 7.23 7.87 7.95 5.89 5.76	8
X=4,9 SI 00-19 C0-39 40-59 60-79 80-99 PCT •85 •10 •20 •20 •50 1.90	00-24 PCT 8.45 11.75 14.36 16.00 12.26 37.16 00-24 6.56 7.45 8.13 7.45	X 9 8	01 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 01 10-14 08 7.39 8.11 7.45 5.15	URNAL 14- FI 12- 17- 17- 15- 11- 25- URNAL 14- 14- 8 7- 7- 6- 8 7- 8- 8- 8- 8- 8- 8- 8- 8- 8- 8- 8- 8- 8-	VA8 1619 1619 1619 1619 1619 1619 1619 161	RIA	TION 2 18-22 PCT 5.38 14.88 18.36 12.56 39.17 TION 18-22 DB 6.38 7.33 8.05 7.48 6.38 7.33 8.05 7.48 6.38 7.33 8.05 7.48 6.38 7.33 8.05 7.48 6.38 7.33 8.05 7.48 6.38 7.33 8.05 7.48 6.38 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.33 8.05 7.38 8.05 7.33 8.05 7.35 7.35 7.35 7.35 7.35 7.35 7.35 7.3	X 8 8	22-02 FCT 1.14 3.26 9.19 15.20 14.04 55.66 2.6 5.2 6.5 7.41 7.78 6.92 4.39	Xas	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41 02-86 08 5.63 7.47 7.59 7.74 6.87 5.75	XS	86-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11 86-10 08 7.23 7.87 7.95 5.89 5.76 8.23	8
SI 00-19 20-39 40-59 60-79 80-49 90-99 PCT .20 .50 1.20 5.00	80-24 PCT 64-5 11.75 14.36 12.26 37.18 80-24 08-56 7.45 6.30 7.34 6.39 3.77	X 9 8	0I 10-14 PCT 20-66 21.76 10-41 13.47 9.30 15.38 0I 10-14 0B 7.45 6.15 5.35 4.04 2.61	URNAL 14- 12- 17- 17- 15- 15- 15- 15- 15- 15- 18- 18- 18- 18- 18- 18- 18- 18- 18- 18	VA 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RIA	TION 18-22 PCT 38-048 14-86 12-56 39-17 TION 18-22 DB 6-38 7-33 8-05 7-48 6-38 5-27	X 8 8	2-02 FC14 3.86 9.19 15.04 55.86 2.8 52 7.41 7.78 6.92 5.81	Xas	02-06 PCT 1-46 4-98 9-63 16-11 14-48 53-41 02-06 08 5-63 7-47 7-59 7-74 5-75	XS	06-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11 86-10 08 7.23 7.87 7.95 5.89 5.76	8
X=4,9 SI 00-19 10-39 40-59 60-79 80-99 PCT • 10 • 20 • 2	80-24 PCT 5 11.75 14.36 12.26 12.26 37.16 80-24 6.56 7.45 8.13 7.32 5.19 3.75 1.32	X 9 8	01 10-14 PCT 20.66 21.76 18:41 13.47 9:38 10-14 DB 7:39 8:11 7:45 5:35 4:04 2:61 1:51 -79 -40	URNAL 14- 12- 17- 17- 15- 11- 25- URNAL 14- X DI B 6- 8- 7- 4- 5- 4- 3- 2- 1-	VA8 151943561 48 2825242633	RIA	TION 2 18-22 PCT 38 9.64 14.88 12.567 3.17 18-22 DB 6.38 7.33 8.05 7.48 5.27 3.86 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 3.80 5.27 5.27 5.20 5.20 5.20 5.20 5.20 5.20 5.20 5.20	X 8 8	2-07 10-16 9-19-15-06 9-19-15-06 2-15-06 2-28-5-41 7-78-6-92 10-16-16-16-16-16-16-16-16-16-16-16-16-16-	Xas	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41 02-86 08 5.63 7.47 7.59 7.59 7.75 4.33 3.12	XS	06-10 PCT 13.37 16.23 18.31 15.46 52 26.11 86-10 7.27 7.95 5.76 4.68 3.23 2.08 3.53	8
SI 00-19 00-39 40-59 60-79 80-99 PCT .85 .10 .20 .20 .20 .20 .20 .20 .20 .2	00-24 PCT 645 11.75 14.36 12.26 37.16 00-24 08.56 7.45 8.30 7.45 8.30 7.32 8.30 8.30	X 9 8	0I 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 0I 10-14 0B 7.39 8.11 7.45 6.15 5.35 4.04 2.61 1.57 .79	URNAL 14- 14- 17- 17- 17- 15- 11- 25- URNAL 14- K DI B 7- 6- 5- 4- 3- 2- 1-	VA8 -18 -18 -18 -18 -18 -18 -18 -18 -18 -1	RIA	TION 2 PCT 3 8 - 6 4 1 8 - 5 6 7 . 3 8 - 1 7 - 3 8 - 1 8 - 2 8 6 - 3 8 7 - 3 8 - 1 8 - 2 8 6 - 3 8 6 -	X 8 8	2-07 10-14 3-14 3-14 3-14 3-14 3-14 3-14 3-14 3	Xas	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41 02-86 08 5.67 7.59 7.77 5.75 4.33 2.18 1.81 9.43	XS	06-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11 96-10 7.27 7.95 5.76 4.68 3.23 2.08 1.53	8
X=4,9 SI 00-19 00-39 40-79 80-49 90-99 PCT .050 1.90 20.00 10.00 20.00 50.00	80-24 PCT 8.45 11.75 14.36 16.00 12.26 37.16 80-24 6.56 7.45 7.34 6.30 5.19 3.75 1.32 8.80	X 9 8	01 10-14 PCT 20.66 21.76 18:41 19:30 15:38 10-14 DB 7:39 6:15 7:45 6:15 5:35 4:04 1:51 •79 •40 •40 •40 •40 •40 •40 •40 •40	URNAL 14- 14- 12- 17- 17- 15- 15- 15- 15- 15- 18- 18- 18- 18- 18- 18- 18- 18- 18- 18	VA8 - 18 - 18 - 18 - 18 - 18 - 18 - 18 -	RIA	TION 2 PCT 38-22 PCT 38-9.64 14.85 14.85 12.56 39.17 TION 2 18-22 DB 6.38 7.35 7.48 5.27 3.65 2.65 2.65 2.65 2.65 2.65	X 8 8	2-02 FC143.86 9.192 15.94 15.96 2.8 9.192 5.41 7.92 1.83 1.83 8.80	Xas	02-06 PCT 1.46 4.98 96-31 16-148 53-41 02-86 53-77 77-75-75 43-77 5-75 4-87 4-87 4-87 4-87 4-87 4-87 4-87 4-87	XS	06-10 PCT 13.37 16.23 18.316 10.52 26.11 86-10 08 7.27 7.87 5.89 5.76 4.68 3.20 1.83 .52	8
SI 00-19 00-39 40-59 60-79 80-99 PCT .85 .10 .20 .20 .20 .20 .20 .20 .20 .2	00-24 PCT 645 11.75 14.36 12.26 37.16 00-24 08.56 7.45 8.30 7.45 8.30 7.32 8.30 8.30	X 9 8	0I 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 0I 10-14 0B 7.39 8.11 7.45 6.15 5.35 4.04 2.61 1.57 .79	URNAL 14- F12- 17- 17- 15- 15- 18- 18- 18- 18- 18- 18- 18- 18- 18- 18	VA8 -18 -18 -18 -18 -18 -18 -18 -18 -18 -1	RIA	TION 2 PCT 3 8 - 6 4 1 8 - 5 6 7 . 3 8 - 1 7 - 3 8 - 1 8 - 2 8 6 - 3 8 7 - 3 8 - 1 8 - 2 8 6 - 3 8 6 -	X 8 8	2-07 10-14 3-14 3-14 3-14 3-14 3-14 3-14 3-14 3	Xas	02-06 PCT 1.46 4.98 9.63 16.11 14.48 53.41 02-86 08 5.67 7.59 7.77 5.75 4.33 2.18 1.81 9.43	XS	06-10 PCT 13.37 16.23 18.31 15.46 10.52 26.11 96-10 7.27 7.95 5.76 4.68 3.23 2.08 1.53	8
SI 00-19 10-39 40-59 60-79 80-99 PCT • 10 • 20 • 20 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90 2.00 1.90	80-24 PCT 5 11.75 14.36 16.00 12.26 37.16 80-24 6.56 7.45 8.30 7.32 8.00 21 21	X 9 8	0I 10-14 PCT 20.66 21.76 18:41 13.47 9.30 15.38 0I 10-14 DB 7.39 8.11 7.45 5.15 4.04 2.61 1.51 .79 .16 0.10 .16 0.10	URNAL 14- 12- 17- 17- 15- 11- 25- 11- 25- 11- 14- 14- 15- 15- 15- 15- 15- 15- 15- 15- 15- 15	V18 1594361 A8 2825240633220251	RIA	TION 2 PCT 38 9.64 14.88 12.56 13.56 7.10 18-22 18-23	X 8 8	2-07-1-6-9-9	Xas	02-06 PCT 1.46 9.63 16.11 14.48 02-86 9.63 16.11 14.48 02-86 03-7-7-7 5.75 4.33 1.89 8.84 -1.89	XS	06-10 PCT 13.37 16.33 16.346 10.52 6.11 06-10 08 7.49 5.64 3.27 7.49 5.63 2.08 1.03 2.08 1.03 2.08 1.03 2.08 1.03 2.08	8
X=4,9 SI 00-19 00-39 40-79 80-49 90-99 PCT .85 .10 .50 1.90 20.00 10.00 20.00 50.00 50.00 50.00 70.00 90.00	80-24 PCT 8.45 11.75 14.36 16.00 12.26 37.18 80-24 6.56 7.45 7.34 6.38 5.19 7.34 6.38 5.19 7.35 6.38 6.28 6.26 6.26 7.45	X 9 8	01: 10-14 PCT 20.66 21.76 13.47 9.30 15.38 10-14 DB 7.39 6.11 7.39 6.15 5.35 4.04 2.61 1.51 .79 .40 .40 .40 .40 .40 .40 .40 .40	URNAL 14- 12- 17- 17- 15- 15- 15- 15- 15- 15- 16- 16- 16- 16- 16- 16- 16- 16- 16- 16	V16 194361 A8 28252406332025130	RIA	TION 2 PCT 38 9.64 14.35 9.64 14.35 12.56 39.17 TION 2 9.64 14.35 12.56 39.17 TION 2 10.32	X 8 8	2-07 10.146 10.126	Xas	02-06 PCT 6-98 96-31 16-148 93-14-148 93-14-148 93-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7-7	XS	06-10 PCT 13.37 16.33 16.346 10.52 6.11 96-10 97.85 10.52 10.53 10	8
X=4,9 SI 00-19 00-39 40-79 80-49 90-99 PCT .85 .10 .50 1.80 2.80 1.80 2.80 10.80 40.80 40.80 95.80	80-24 PCT 8.45 11.75 14.36 16.06 12.26 37.16 80-24 6.56 7.45 7.34 6.30 5.19 2.55 1.32 8.00 29 71 -1.44 -2.85	X 9 8	01 10-14 PCT 20.66 21.76 18.41 13.47 9.38 15.38 10-14 DB 7.39 8.11 7.45 6.15 5.35 4.04 2.61 1.79 .48 8.10 -1.80 -2.39	URNAL 14- F12-17- 17- 17- 15- 12- 18- 18- 18- 18- 18- 18- 18- 18- 18- 18	V10 154561 A8 28252406332925137	RIA	TION 2 PCT 38 9.64 14.85 9.64 14.85 12.57 118-22 9.64 14.85 12.56 39.17 18-28 12.56	X 8 8	2-07146922 2-07146922 2-07146922 3-19246 3-19246 3-19246 3-1922 3-19246 3-1924	Xas	02-06 PCT 6-98 9-53 14-41 9-63 14-41 9-63 14-41 9-77 9-77 9-77 9-77 9-77 9-77 9-77 9-7	XS	06-10 PCT 13.37 16.23 18.346 10.52 26.11 96-10 26.11 96-10 27.87 5.76 95-76 3.28 1.83 2.08 2.08 2.08 2.08 2.08 2.08 2.08 2.08	8
X=4,9 SI 00-19 00-39 40-79 80-49 90-99 PCT .85 .10 .50 1.90 20.00 10.00 20.00 50.00 50.00 50.00 70.00 90.00	80-24 PCT 8.45 11.75 14.36 16.00 12.26 37.18 80-24 6.56 7.45 7.34 6.38 5.19 7.34 6.38 5.19 7.35 6.38 6.28 6.26 6.26 7.45	X 9 8	01: 10-14 PCT 20.66 21.76 13.47 9.30 15.38 10-14 DB 7.39 6.11 7.39 6.15 5.35 4.04 2.61 1.51 .79 .40 .40 .40 .40 .40 .40 .40 .40	URNAL 14- 12- 17- 17- 15- 15- 15- 15- 15- 15- 16- 16- 16- 16- 16- 16- 16- 16- 16- 16	V16 194861 A8 282524063320251375	RIA	TION 2 PCT 38 9.64 14.35 9.64 14.35 12.56 39.17 TION 2 9.64 14.35 12.56 39.17 TION 2 10.32	X 8 8	2-T14692 2-T14692 2-T14692 3-192 3-192 3-192 15-066 3-192 15-083 1-092 1-092 1-092 1-092 1-092 1-092 1-092 1-092	Xas	02-06 PCT 6-4-98 9-63 16-44 9-63 16-44 9-63 16-44 9-63 1-84 9-63 1-84 1-84 1-84 1-84 1-84 1-84 1-84 1-84	XS	06-10 PCT 13.37 16.33 16.346 10.52 6.11 96-10 97.85 10.52 10.53 10	8
X=4,9 SI 00-19 C0-39 40-79 60-79 90-99 PCT .85 .10 .50 1.90 20.00 10.00 20.00 50.00 50.00 50.00 70.00 90.00 90.00 90.00 90.00	80-24 PCT 545 11.75 11.75 16.026 37.18 80-24 6.55 7.34 80-25 7.34 80-29 29 29 29 29 29 29 29	X 8 8	01 10-14 PCT 20.66 21.76 13.47 9.30 15.38 10-14 DB 7.39 6.15 5.35 6.15 5.35 4.04 1.51 .79 .40 .10 .10 .10 .10 .10 .10 .10 .1	URNAL 14-1 17-117-117-117-117-117-117-117-117-11	V16 194861 A8 2825240633292519752	RIA	TION 2 PC 38 9.648 18.366 9.648 18.366 39.17 TION 2 B 38 37.48 6.37 6.38 7.48 6.37 6.38 7.48 6.37 6.38 7.48 6.37 6.38 7.48 6.38 6.37 6.37 6.37 6.37 6.37 6.37 6.37 6.37	X 8 8	2-07146922 2-07146922 2-07146922 3-19246 3-19246 3-19246 3-1922 3-19246 3-1924	X 3 5 8	02-06 PCT 64-98 96-31 16-41 96-31 16-42 96-31 16-42 97-77 97	XSBB	06-T 13.32 16.32 18.452 26.11 96-11	8
X = 4 i 9 SI = 19 CO = 19 CO = 39 40 = 79 80 = 79 90 = 9 PCT = 85 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20	80-24 8.45 11.75 14.36 16.06 12.26 37.16 90-24 6.56 7.32 6.38 7.33 6.38 7.32 6.38 7.34	X 9 8 9	01 10-14 PCT 20.68 21.76 18.47 13.47 15.38 15.38 10-14 DB 7.39 15.35 4.04 2.51 1.51 .79 .48 0.16 34	UR 14- 125- 125- 125- 125- 125- 125- 125- 125	VAS 194361 AS 282524063320251375215	RIA	TION 22 85648 866 87 89 148 866 87 89 148 866 87 87 87 87 87 87 87 87 87 87 87 87 87	X 8 5 8	2 C C C C C C C C C C C C C C C C C C C	X 8 6 8	02-06 PCT 66 98 96.118 96.118 96.118 96.118 96.118 97.77.77.5.73 21.893 8-4863-4863-4863-4863-4863-4863-4863-486	XSDS	0 PC 37 16.23 18.346 10.52 18.452 18.	8
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20-39	4.64		15.60		19.49		11.77		7.04		15.68		16.23
60-79	28.92		25.92		27.59		28.79		27.22		35.17		28.95
80-89	23.46		19.77		23.12		24.84		24.68		15.68 35.17 21.95 23.14		22.11
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2.80	4.89		4.85		4.59		3.77		3.56		3.39		3.23
10.00	2.48		2.40		2.34		2.66		2.64		2.37		2.23
20.00	1.43		1.34		1.35		1.56		1.70		1.39		1.27
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88.80	-1.55		-1.45		-1.46		-1.70		-1.66		-1.50		-1.38
90.00	-2.82		-2.71		-2.65		-3.05		-3.29		-4.87		-2.56
95.88	-4.30 -6.52		-4.60		-F.16		-6.93		-7.29		-6.16		-5.89
99.00	-8.39		7.50 7.50		-8.01		-8.82		- 1.19		-8.00		-3.87 -5.89 -7.69 -9.56
99.50	-10.34		-10.31		-9.91		-10.83		-11.29	_	-9.90		-9.56
99.80	-13.64	_	-13.64 -10.35	_	-12.63		-16.12	A	-15.14	A	-12.76	A	-12.00 B
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THULE K=4,° SI 00-19 20-39 40-59 60-79 89-89 90-99	90-24 PCT 90-01 1.55 7.43 30.40 31.61 29.02	X B	CI 10-14 PCT U.JO 2.34 1.47 26.47 33.02 35.29 CI 10-14 DB	UF X B	ALL NAL VA 14-18 PCT 8.00 1.33 9.33 45.33 22.67 21.33	DI RI	ATA ATION 18-22 PCT 0.00 0.00 7.59 30.38 32.91 29.11	1	22-02 PCT 0.00 0.90 12.55 32.55 29.19		02-06 PCT 0.00 4.62 6.15 23.85 23.85	X B	06-10 PCT 0.00 0.00 4.35 27.17 29.35 39.13
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THULE K=4,° SI 00-19 20-39 40-59 60-79 80-89 90-99 PCT 05 • 10 • 20 • 20 2-00	90-24 PCT 0.00 1.55 7.43 30.40 31.61 29.02 00-24 00-24 7.39 8.06 7.20 6.14 5.05	¥ 8 8	CI 10-14 PCT JO 2.347 26.47 26.47 33.82 GI 10-8 37.16 8.90 7.40 5.30	UF X B B	ALL 14-18 PCT 8-10 1.33 9-33 45-33 22-67 21-33 22-67 21-33 27-78 6-83 5-65 6-83 9-64	RI X B	ATA ATION 18-22 PCT 0.00 0.00 7.59 30.38 32.91 29.11 ATICN 18-22 D9 7.38 8.06 7.21 6.15 5.06	X 8 8 8	22-02 PCT 0.00 0.00 12.59 32.59.19 25.19 22-02 08 7.57 7.97 5.95 4.87	XBB	2-06 PCT 0.00 4.62 6.15 23.85 38.46 26.92 2-06 UB 5.24 7.49 8.02 7.16 6.10 5.01	X B B	06-10 PCT 0.00 0.00 4.35 27.17 29.35 39.13 86-10 DB X 5.77 B 6.96 B 8.00 B 7.48 6.51
THULE K=4,° SI 00-19 20-39 40-59 60-79 88-89 90-99 PCT 5 • 20 • 50 • 20 • 50 • 50	90-24 PCT 0.00 1.55 7.43 30.40 31.61 29.02 00-24 D6 4.94 7.39 8.06 7.20 6.145 5.373	¥ 0 8	CI 10-14 PCT JO 2.347 26.47 26.47 23.82 35.82 CI 10-1 93 7.40 6.40 5.91 8.90 5.91	UF X B B	ALL NAL VA 14-18 PCT 8-10 1-33 9-33 45-33 22-67 21-33 RMAL VA 14-16 08-65 7-70 7-86 6-83 9-69 4-3-37	RI X B	ATA ATION 18-22 PCT 0.00 7.59 35.38 32.91 29.11 ATICN 18-22 DB 4.90 7.38 8.86 7.21 6.15 5.36	x 8 8 8	22-02 PCT 0.00 0.00 12.55 32.55 29.63 25.19 22-02 09 5.38 7.57 7.65 5.65	XBB	2-06 PCT 0.00 4.62 6.15 23.45 23.45 26.62 2-06 UB 5.24 7.16 6.10 5.71	X B B	06-10 PCT 0.00 0.00 0.035 27-17 29-35 39-13 96-10 08 X 5.77 B 8-00 B 7-48 6-51 5-44
THULE, SI 108-19 20-39 40-59 60-79 88-99 PCT	20-24 PCT 0.00 1.55 7.43 30.40 29.02 00-24 00-24 7.39 8.06 5.05 3.66	¥ 8 8	CI 10-14 PCT JO 2.347 26.47 26.47 25.47 26.47 26.47 26.47 26.47 26.47 26.47 27.40 27.40 27.40 27.40 27.40	UF X B B	ALL 14-18 PCT 8-10 1.33 9-33 45-33 22-67 21-33 22-67 21-33 27-78 6-83 5-65 6-83 9-64	RI X B B	ATA ATION 18-22 PCT 0.00 0.00 7.59 30.38 32.91 29.11 ATICN 18-22 D9 7.38 8.06 7.21 6.15 5.06	x 9 8 8	22-02 PCT 0.00 0.00 12.59 32.59.19 25.19 22-02 08 7.57 7.97 5.95 4.87	XBB	2-06 PCT 0.00 4.62 6.15 23.85 38.46 26.92 2-06 UB 5.24 7.49 8.02 7.16 6.10 5.01	X B B	06-10 PCT 0.00 9.00 4.35 27.13 39.13 96-18 X 8 6.96 8 7.48 8.51 5.48 4.092
THULE K=4,° SI 00-19 20-39 40-59 60-79 88-89 90-99 PCT 5 • 20 • 50 • 20 • 50 • 50	90-24 PCT 0.00 1.55 7.43 30.40 31.61 29.02 00-24 D6 4.94 7.39 8.06 7.20 6.145 5.373	¥ 0 9 8	CI 10-14 PCT JO 2.347 26.47 26.47 23.82 35.82 CI 10-1 93 7.40 6.40 5.91 8.90 5.91	UF X B B	ALL  INAL VA  14-18 PCT  9.00  1.33 9.33 45.33 22.67 21.33 22.67 21.33 22.67 21.33 22.67 21.33 22.67 21.33 22.67 21.33 22.67 21.33	PI RI X B B	ATA ATION 18-22 PCT 0.00 7.59 30.38 32.911 29.11 ATICH 22 DB 4.90 7.38 8.86 7.21 6.15 5.86 3.75 2.66	x 9 8 8	22-02 PCT 00.00 0.00 12.55 32.55 29.63 25.19 2-02 208 5.57 7.65 4.87 3.54	XBB	02-06 PCT 0.00 4.62 6.15 23.86 26.92 2-06 108 5.24 7.49 8.02 7.49 8.02 7.10 5.01 3.66	X B B	06-10 PCT 0.00 9.00 4.35 27.35 39.13 96-10 29.69 86.96 88.00 86.96 88.00 86.96 88.00 86.96 88.00 80 80 80 80 80 80 80 80 80 80 80 80 8
THULE, "  K = 4, "  S I	90-24 PCT 0.00 1.55 7.43 30.40 31.61 29.02 00-24 5.39 8.06 7.20 6.145 3.73 2.66 1.59	¥ 0 8	CI 10-14 PCT JO 2.347 26.477 26.477 25.429 CI 10-14 10	UF X B B	ALL  INAL VA  14-18 PCT  8-10 1.33 9.33 45.33 22.67 21.33 22.67 21.33 27.86 6.83 5.66 3.37 2.39 4.63 3.37	PI RI X BB	ATA ATION 18-22 PCT 0.80 0.60 7.59 30.38 32.91 29.11 ATICN 18-22 D8 4.90 7.38 8.86 7.21 6.15 5.86	x 9.8 B	22-02 PCT 0 0.00 12.59 32.59 25.19 22-02 25.19 22-02 35.77 7.95 54.87 3.54 2.52	XBB	02-06 PCT 0.00 4.62 6.15 23.85 26.92 2.06 2.08 5.24 7.49 8.02 7.10 5.01 3.71 2.59	X B B	06-10 PCT 0.00 0.00 27-37 29-35 39-13 96-10 25-77 86-10 86-1
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